

# ***Headquarters U.S. Air Force***

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*Integrity - Service - Excellence*

## **The BIOSCREEN Natural Attenuation Model**



**U.S. AIR FORCE**

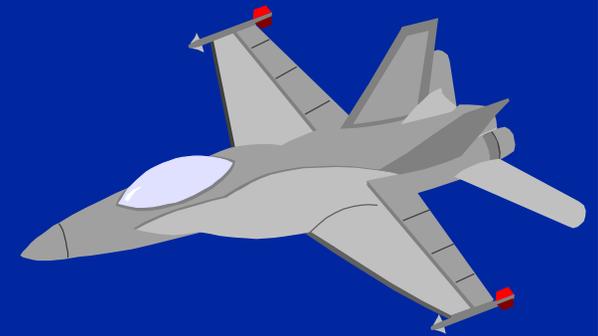
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**Charles J. Newell, Ph.D., P.E.  
Groundwater Services, Inc.  
Jan. 31, 2001**

# Team Members and Funding

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- **K. McCleod**  
*GSI / Radian*
- **Jim Gonzales, Ross Miller**  
*AFCEE Tech Transfer Division*

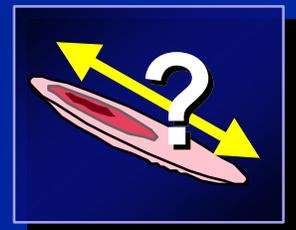


*Funded by AFCEE Tech Transfer Division*

# Talk Outline

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- **INTRODUCTION**
- *BIOSCREEN Natural Attenuation Model*
- *BIOCHLOR Natural Attenuation Model*
- *BIOPLUME III Natural Attenuation Model*



# BTEX Plumes vs. Other Plumes

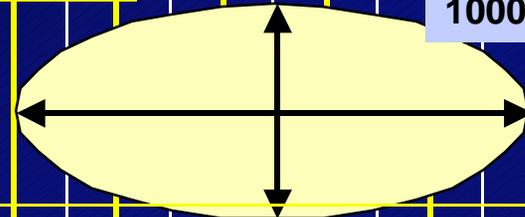
## MEDIAN PLUME DIMENSIONS

**BTEX Plumes  
at Retail Sites**  
(42 Sites)



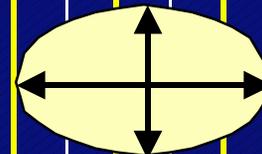
213 ft x 150 ft

**Chlorinated  
Ethene Plumes**  
(88 Sites)



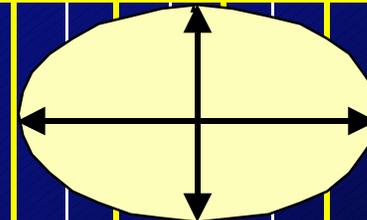
1000 x 500 ft

**Other Chlor.  
Solvent Plumes**  
(29 Sites)



500 ft x 350 ft

**Chloride, Salt  
Water Plumes**  
(25 Sites)



700 ft x 500 ft

0 200 400 600 800 1000  
Feet

Data from  
HGDB Hydrogeologic  
Database

(Newell et al., 1990;  
API, 1989)

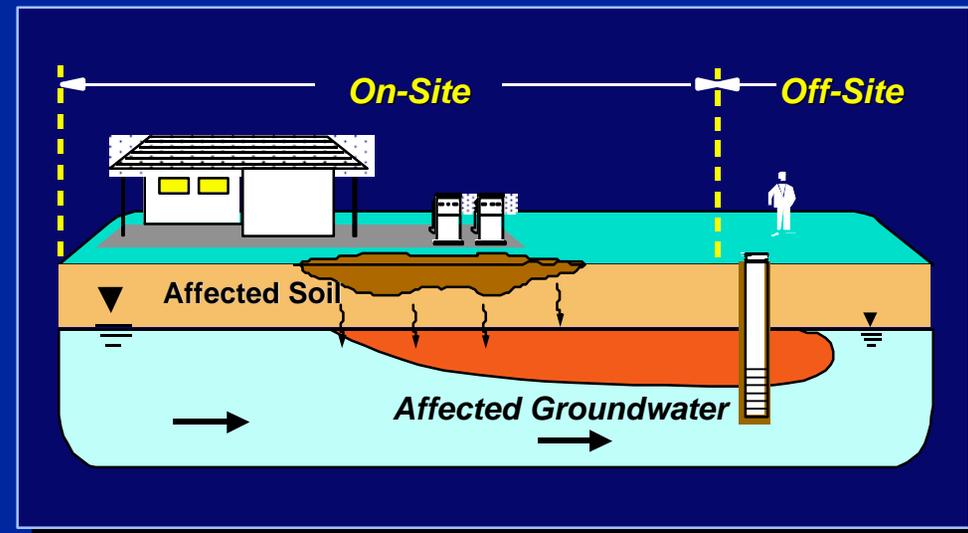
# BIOSCREEN Processes

## *Key Concept:*

- Applies to Most Types of Sites Except Some of Biodeg.

## *Key Processes:*

- Advection
- Dispersion
- Adsorption
- Biodegradation



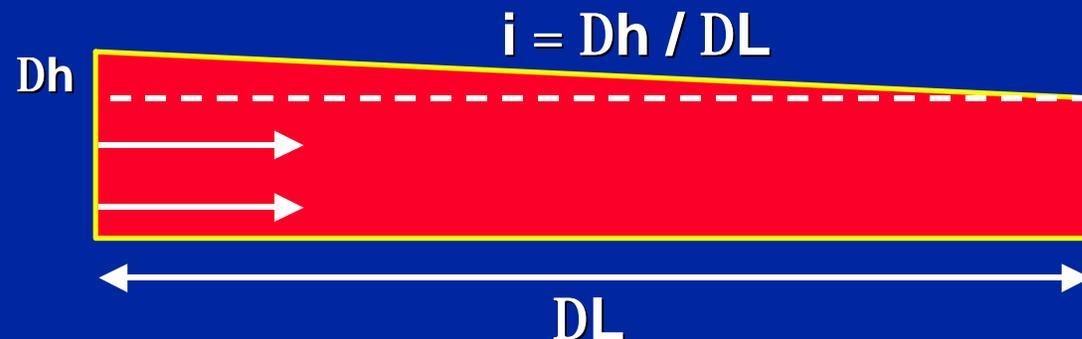
# Groundwater Transport Processes

## Advective Transport

“Advection” refers to the bulk motion of a fluid.

$$V_d = K i$$

$$V_s = \frac{K i}{n}$$



$V_d$  = Darcy velocity (cm/s, ft/d, etc.)

$V_s$  = Seepage velocity [cm/s, ft/d, etc.]

$K$  = hydraulic conductivity [cm/s, ft/d, etc.]

$i$  = hydraulic gradient [cm/cm, ft/ft, etc.]

$n$  = effective soil porosity (dim)

# Parameters for Advection

## Parameter

## Measure?

## Estimate?

- Hydraulic Conduct.
- Hydraulic Gradient
- Effect. Porosity

Slug, Pump Test

$5 \times 10^{-3}$  cm/sec  
(HGDB National Median)

Pot. Map

0.006 ft/ft  
(HGDB National Median)

Lab Test

ASTM: 0.38  
Others: 0.25



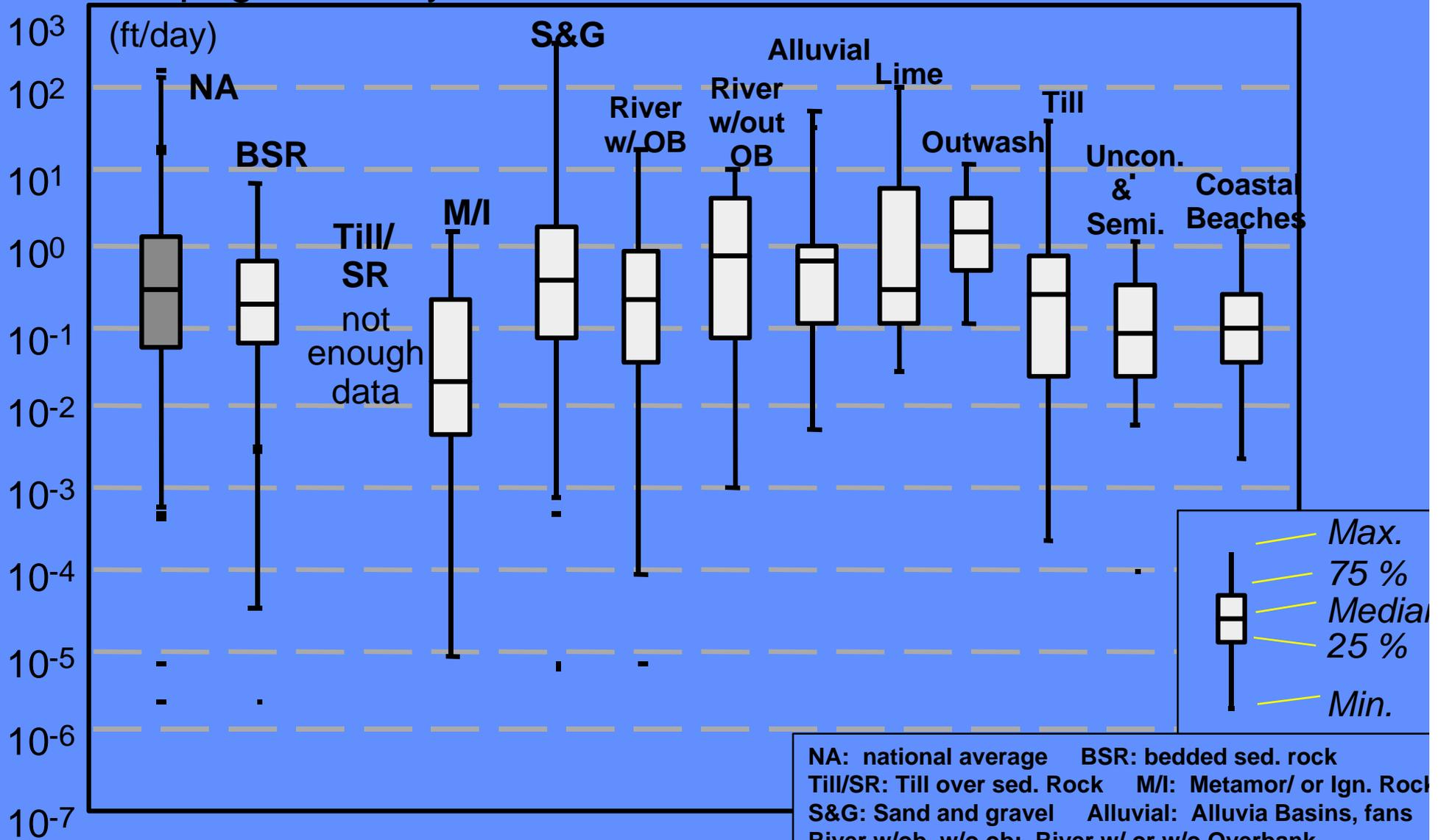
HGDB National Median  
Seepage Velocity:

25%: 30 ft/yr

Median: 88 ft/yr

75%: 400 ft/yr

# Seepage Velocity



Source: Newell et al. 1990; Weiedemeier et al. 1999

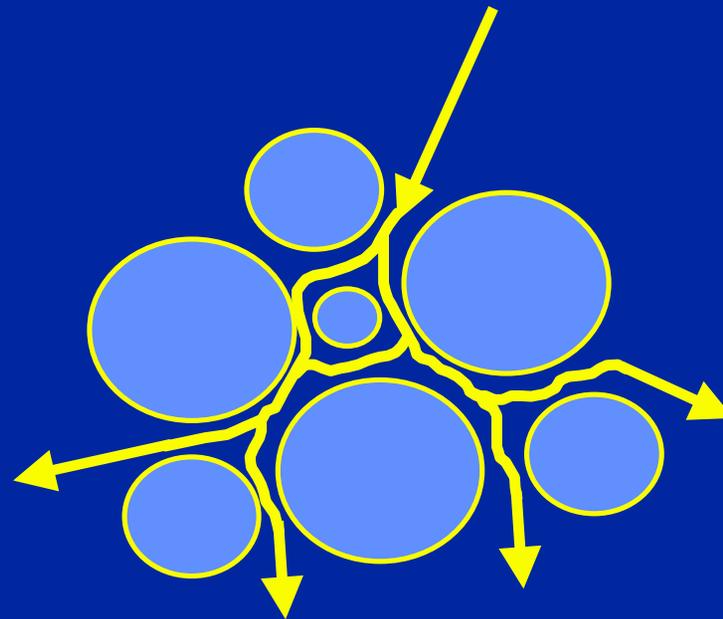
NA: national average    BSR: bedded sed. rock  
 Till/SR: Till over sed. Rock    M/I: Metamor/ or Ign. Rock  
 S&G: Sand and gravel    Alluvial: Alluvia Basins, fans  
 River w/ob, w/o ob: River w/ or w/o Overbank  
 Lime: Solution limestone    Till: Till and Till over outwa  
 Uncon & Semi. Unconsol. and semicons. shallow

# Groundwater Transport Processes

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## Dispersion

“Dispersion” refers to the in-situ micro-scale mixing that results as a fluid flows through a porous medium.



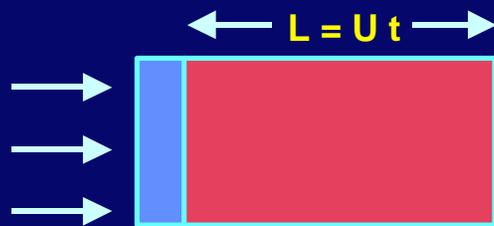
# Hydrodynamic Dispersion

The extent of spreading, or mixing, caused by dispersion is characterized by a “dispersion coefficient,”  $D$  [ $\text{ft}^2/\text{d}$ ,  $\text{cm}^2/\text{s}$ , etc.],

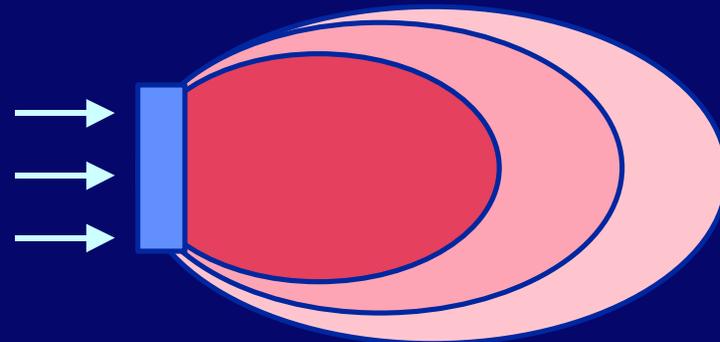
where

{ width of spreading in direction  $i$  } →

Is related to the seepage velocity and “dispersivity”



Transport at time  $t$   
without dispersion



Transport at time  $t$   
with dispersion

# Dispersivities in Three Directions

Dispersion coefficients are typically expressed as the product of a “dispersivity” and the groundwater velocity  
VS:

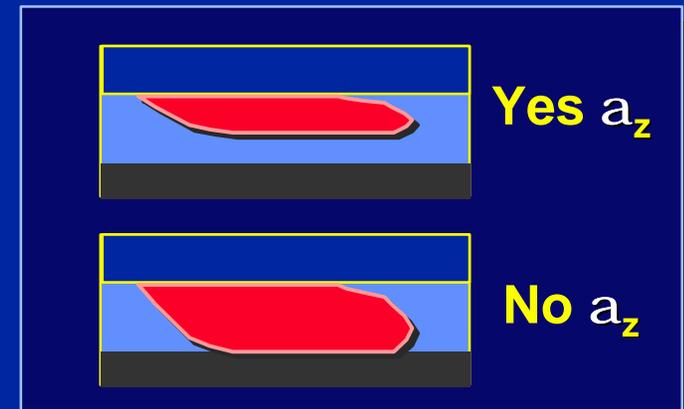
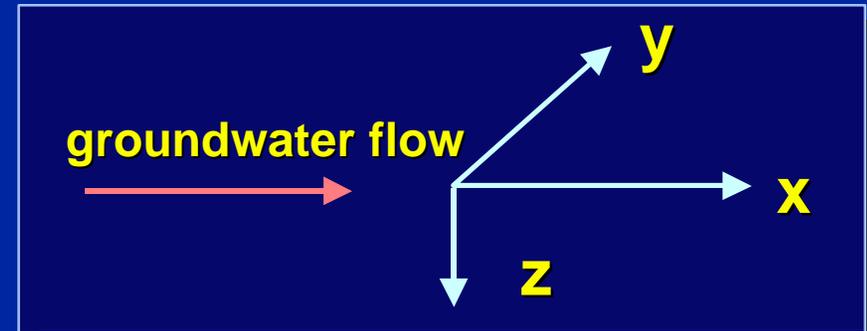
$a_x$  = longitudinal (x-direction) dispersivity

$a_y$  = transverse (y-direction) dispersivity

$a_z$  = vertical (z-direction) dispersivity

*(Note: If plume extends throughout vertical extent of the saturated zone, there is no vertical dispersion and  $a_z$  is a very low number.)*

REQUIRED DATA:  $a_x$ ,  $a_y$ ,  $a_z$  [ft, m, cm, etc.]

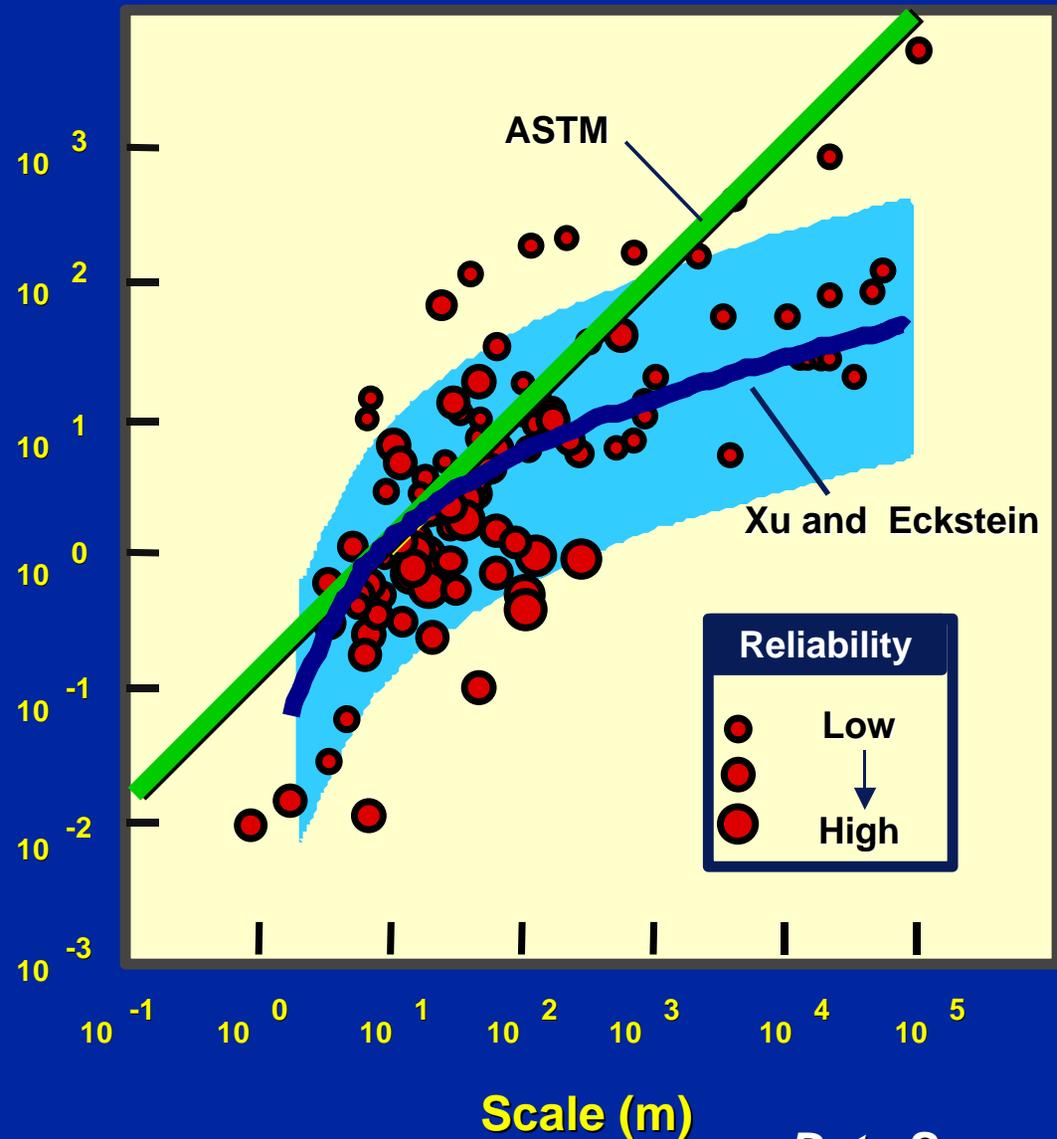


# Estimating Dispersivity

Longitudinal Dispersivity (m)

Dispersivity is correlated to “scale”

Dispersivity is **NOT** strongly correlated to permeability, aquifer material, grain size, other geologic factors



# Hydrodynamic Dispersion

Rules of Thumb are usually used to estimate the dispersivities - and are based on size of plume, not geology

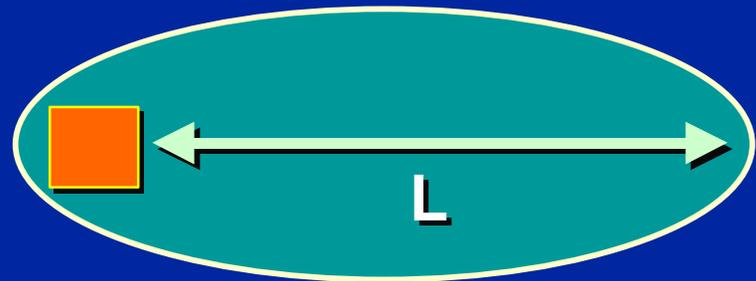
$$a_x = L/10$$

$$a_x = 0.83[\log(L)]^{2.414} \quad (\text{Xu/Eckstein relationship})$$

$$a_y = a_x/3 \text{ or } a_x/10$$

$$a_z = a_y/10$$

**L = distance away from source**



# Parameters for Dispersion

## Parameter

- Longitudinal Dispersivity
- Transverse Dispersivity
- Vertical Dispersivity

## Measure?

*no*

*no*

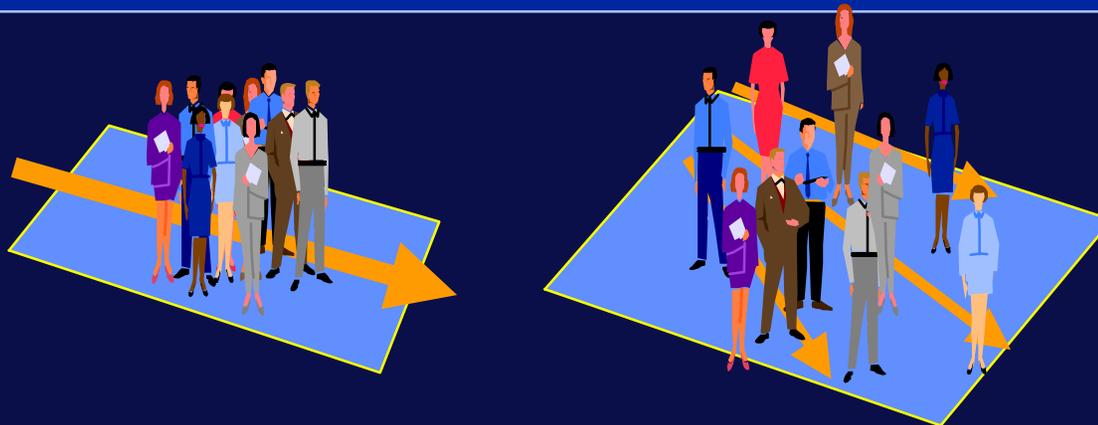
*no*

## Estimate?

ROT / 10- 70 ft

10% of Long.D.

$10^{-99}$  or 10% of  
Trans. D.



**Very Rough ROT:**

*Dispersion not  
important if plume <  
1000 ft long*

# Groundwater Transport Processes

## Sorption Effects

Due to sorption to naturally occurring carbon on the aquifer matrix, dissolved hydrocarbons move at a slower speed than that of the bulk groundwater movement.

$$V_{hc} = \frac{V_s}{R}$$

$$R = 1 + \frac{k_d r_s}{n}$$

$V_{hc}$  = contaminant velocity [cm/s, ft/d, etc.]

$V_s$  = groundwater seepage velocity [cm/s, ft/d, etc.]

$R$  = retardation factor

$k_d$  = soil-water distribution coefficient [(mg/kg-soil)/(mg/l-H<sub>2</sub>O)]

$r_s$  = soil bulk density [g<sub>dry</sub>-soil/cm<sup>3</sup>-soil]

$n$  = effective soil porosity [l-H<sub>2</sub>O/l-soil]



# Groundwater Transport Processes

## Where Does $k_d$ Come From?

- Estimation of distribution coefficient ( $k_d$ ) for organic chemicals.

$$k_d = K_{oc} \times f_{oc}$$

$$k_d = \frac{C_s}{C_w}$$

$k_d$  = soil-water distribution coefficient ([mg/kg-soil]/[mg/l-H<sub>2</sub>O])

$f_{oc}$  = fraction of organic **carbon** in soil (unitless)

$K_{oc}$  = organic carbon partition coefficient (mg/mg/mg/l)

- estimated using regression equations
- obtained from the literature, reference books, chemical databases

# Parameters for Adsorption

## Parameter

## Measure?

## Estimate?

- Bulk Density ( $r_b$ ), Porosity
- Fraction organic carbon (foc)
- Partition Coefficient (koc)

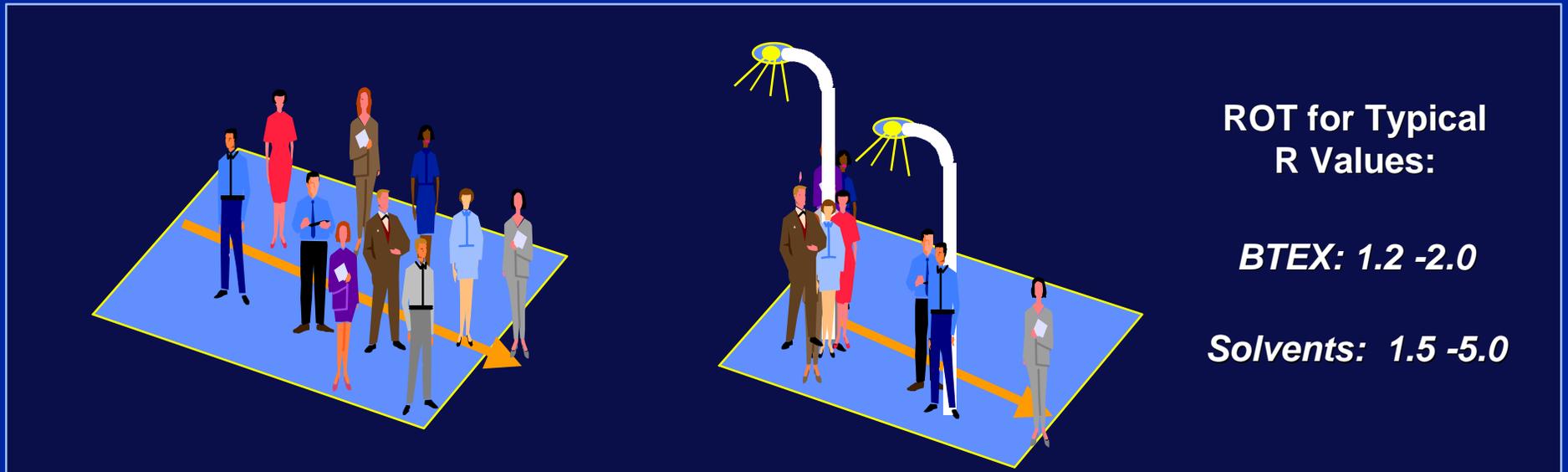
Not typical  
**Soil sample**  
(clean part of water-bearing zone)

No

$r_b$ : 1.7 g/cm<sup>3</sup>

ROT: 0.001 g/g

**Book value:**  
1-500 L/kg



# Groundwater Transport Processes

## Biodegradation

Indigenous micro-organisms are capable of degrading most fuel-range petroleum hydrocarbons. These organisms are typically found at cell densities of  $10^4$  -  $10^6$  cells/g-soil (based on plate counts).

For example, for the aerobic reaction:



Here, the hydrocarbon acts as an electron donor, an energy source and a source of carbon for growth of new bacteria cells.

# First Order Decay Model

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- Simplification of M-M Model
- Fewer parameters required
- Mathematically simple
- Assumptions:  $C \ll K_s$ ,  $X$  is constant

$$\text{Rate} = \frac{-k_s X C}{K_s + C}$$



$$\text{Rate} = -I C$$

# Groundwater Transport Processes

## Biodegradation: First Order Decay

Most hydrocarbon degradation reactions are treated as being “first-order” reactions:

$$\left\{ \begin{array}{l} \text{rate of} \\ \text{disappearance} \end{array} \right\} \text{ is proportional to } \left\{ \begin{array}{l} \text{concentration of} \\ \text{hydrocarbon} \end{array} \right\}$$
$$\text{rate} = - \lambda C$$

$\lambda$  is called a “rate constant.”

# Groundwater Transport Processes

## First-Order Decay Model

$$\frac{dC}{dt} = -lC$$

$$C_{(t)} = C_o e^{(-lt)}$$

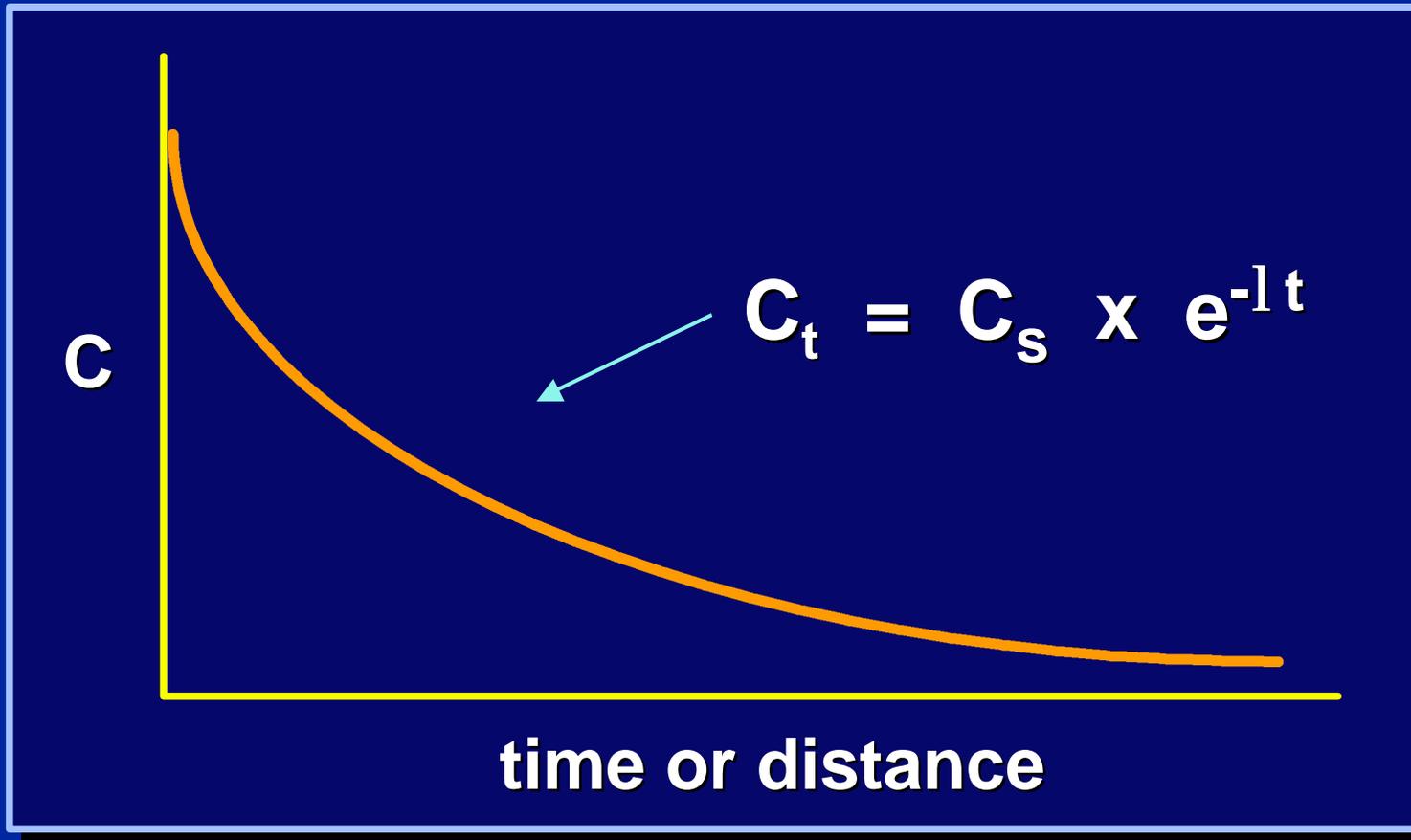
$C_{(t)}$  = concentration at time t (mg/L)

$C_o$  = initial concentration (mg/L)

$l$  = first order decay rate constant (1/t)

# First Order Decay Model

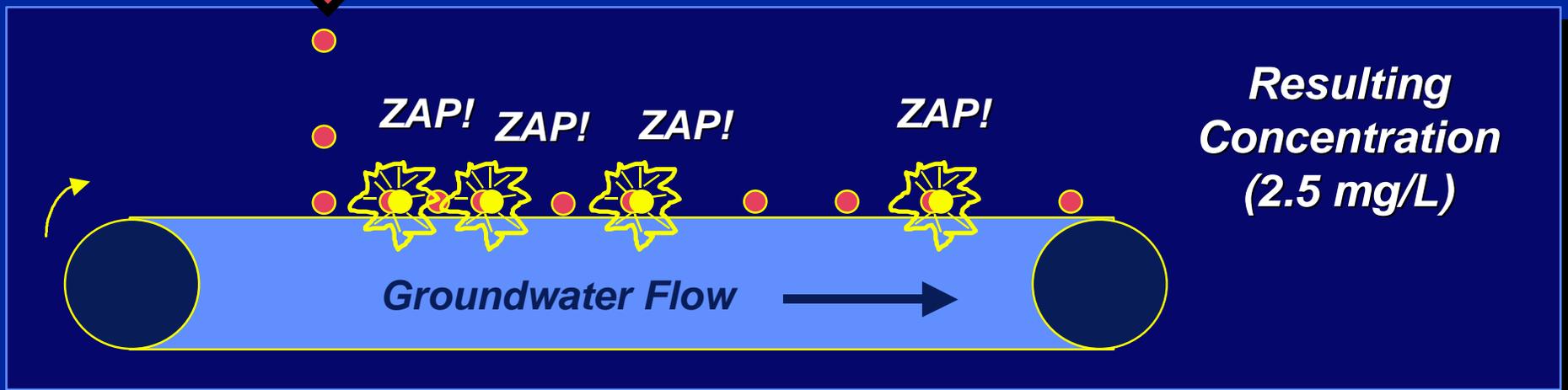
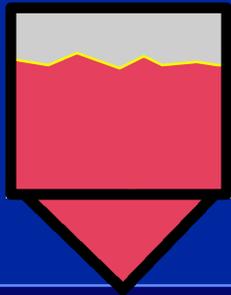
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# First Order Decay Biodegradation

## Conceptual Model

*Observed Source Zone  
Concentration  
(5 mg/L)*



# Biodegradation Half-Life

The half life of a chemical is defined as the time it takes for the first order reaction to transform half of the initial mass of the chemical. If  $C(t)/C_0$  is replaced with 0.5, then:

$$t_{\text{half}} = -(\ln 0.5)/l \quad \text{or} \quad t_{\text{half}} = \boxed{0.693/l}$$

$t_{\text{half}}$  = half life of the chemical (days). Example:

$$l = 1.386/\text{yr} \quad t_{\text{half}} = 0.5 \text{ yrs}$$

and

$$l = 2.77/\text{yr} \quad t_{\text{half}} = 0.25 \text{ yrs}$$

# Parameters for Biodegradation

## Parameter

- First Order Decay Rate Constant ( $k$ )

## Measure?

Calibrate  
to site  
data

## Estimate?

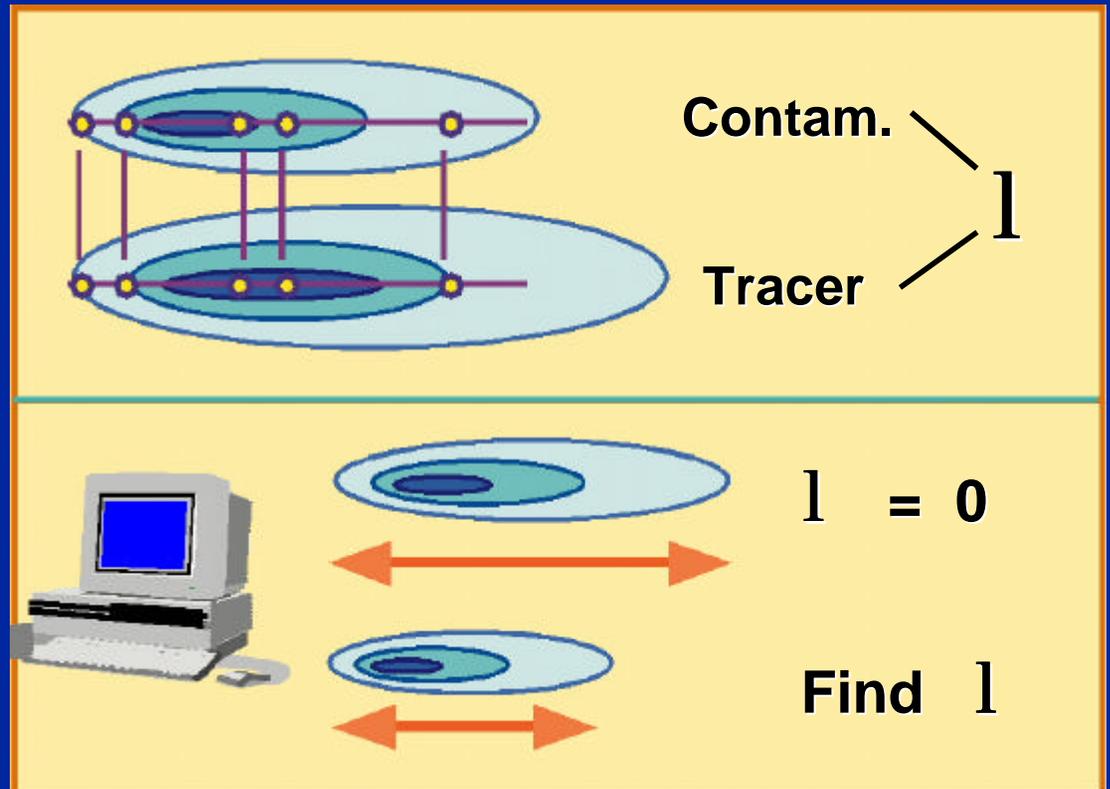
Literature  
values



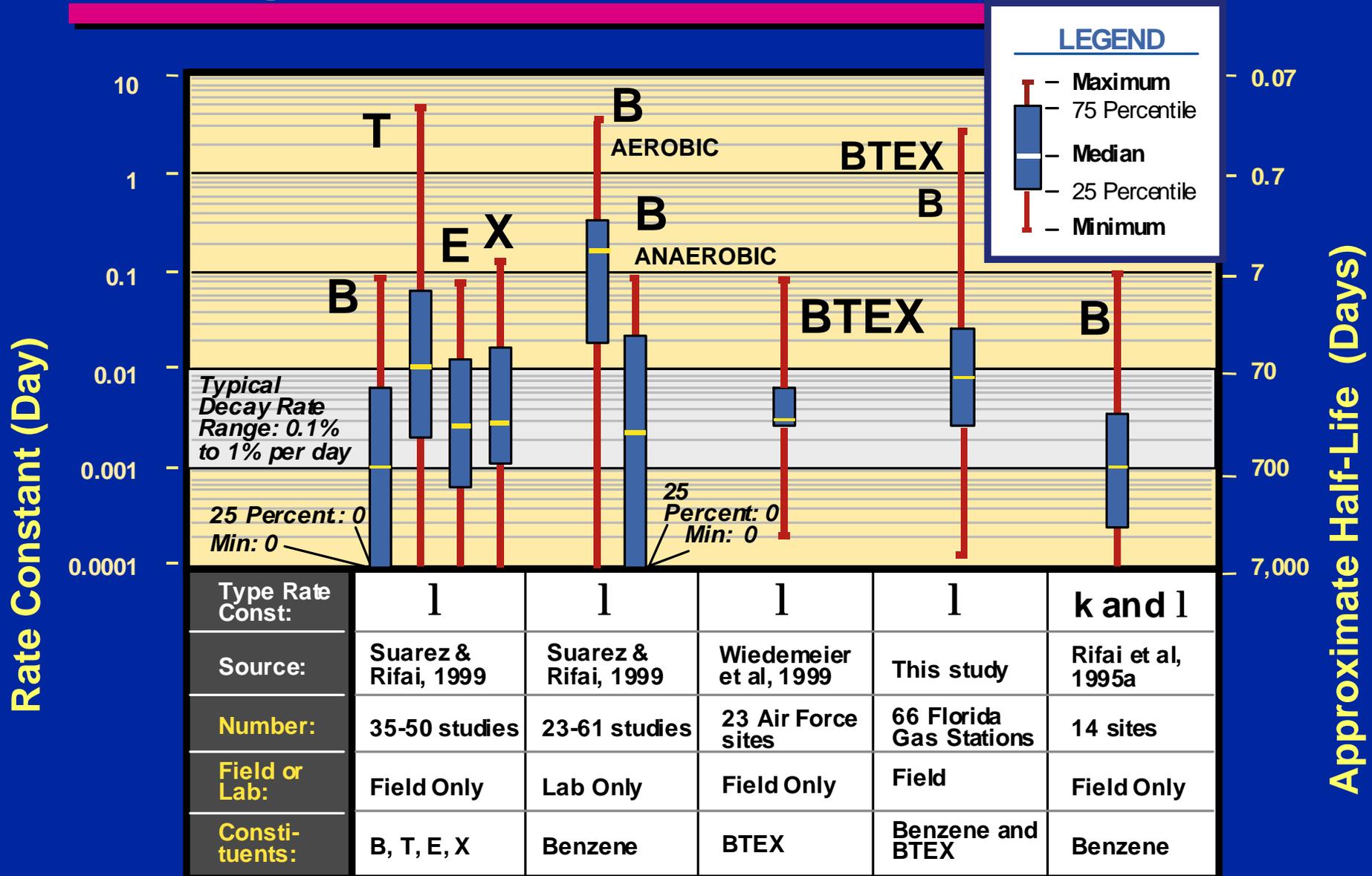
# ***Type of Rate: Biodegradation Rate Constant ( $\lambda - l$ )***

***Represents:***  
**Biodegradation rate of dissolved constituents. Used to estimate how far a plume will migrate.**

**It should not be used to estimate the time required to reach a remediation goal.**



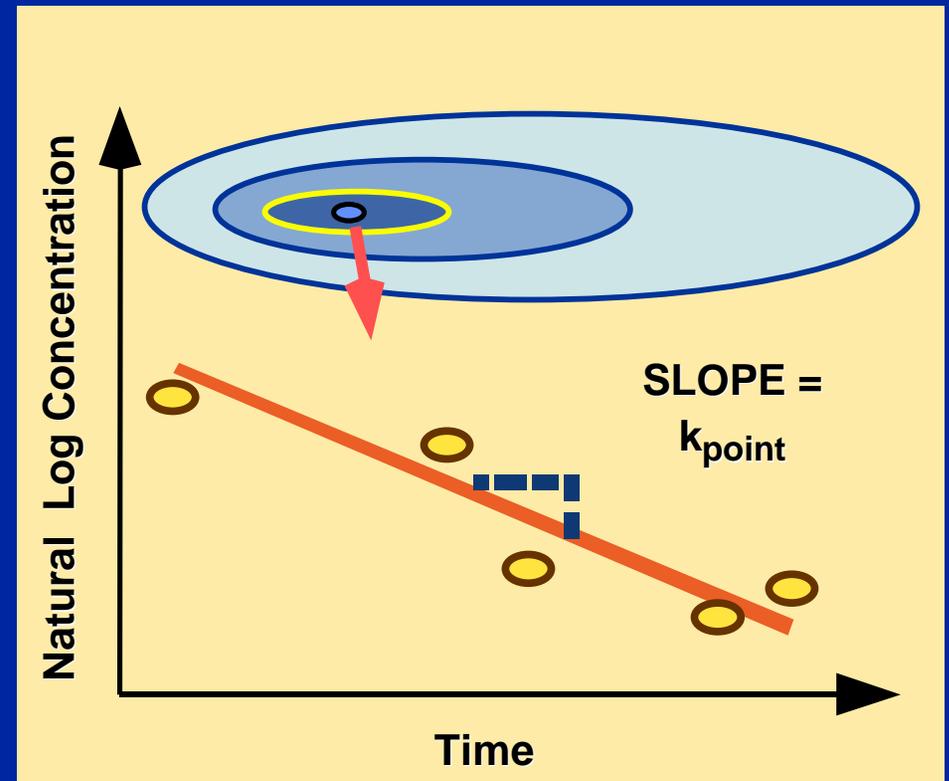
# Biodegradation Rate Constants



# Type of Rate: Point Decay Rate ( $k_{\text{point}}$ ) Constant

**Represents:**  
Primarily change in source strength over time (also called  $k_{\text{source}}$ ).

**It should not be used to describe biodegradation in models!**



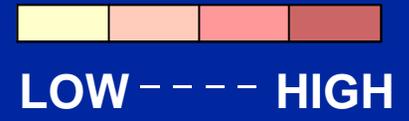
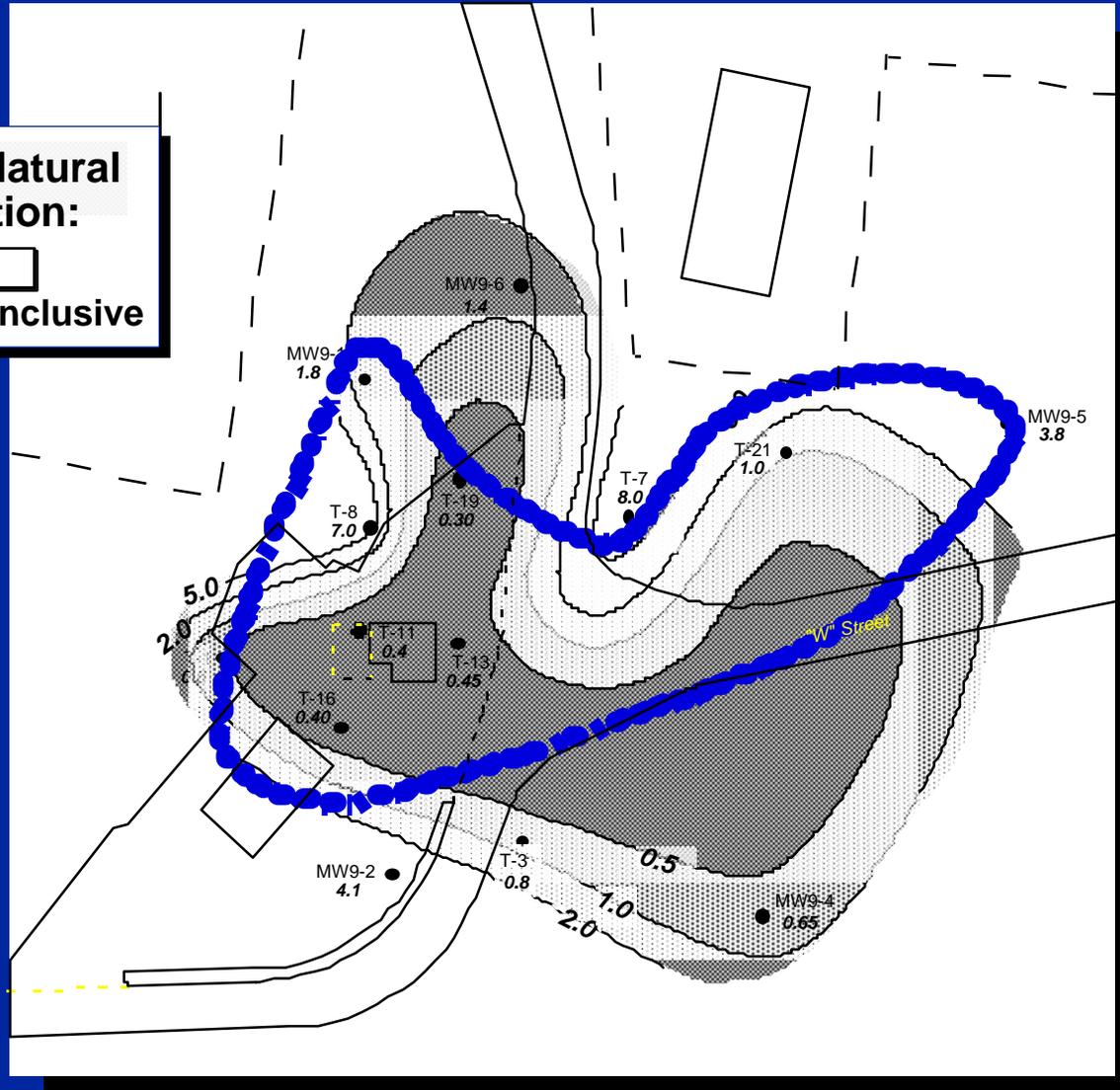
# Keesler Air Force Base



# Dissolved Oxygen in Groundwater (mg/L)

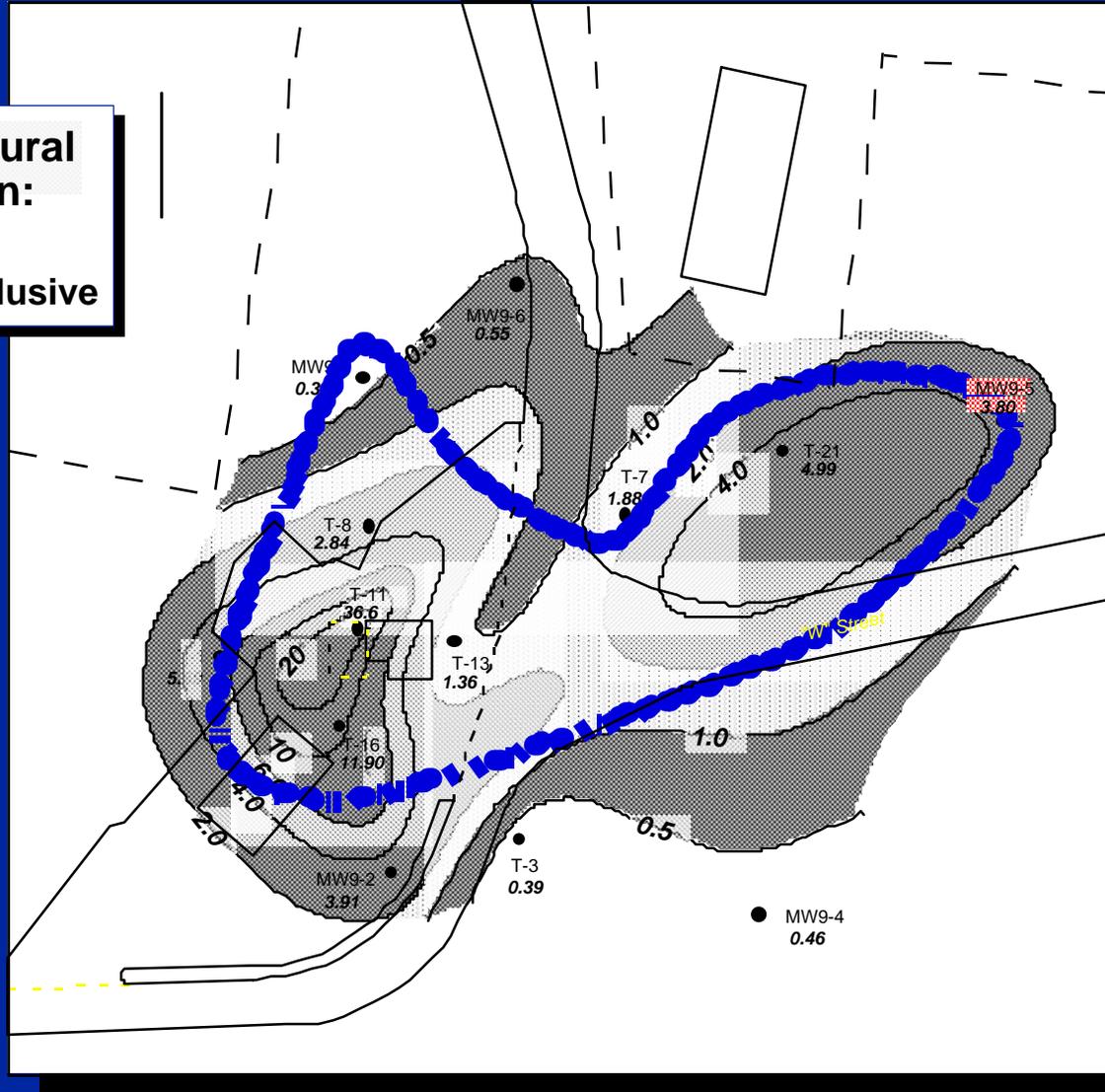
**Supports Natural Attenuation:**

Yes No Inconclusive



# Dissolved Ferrous Iron in Groundwater (mg/L)

Supports Natural Attenuation:  
 Yes    No    Inconclusive

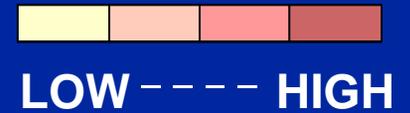
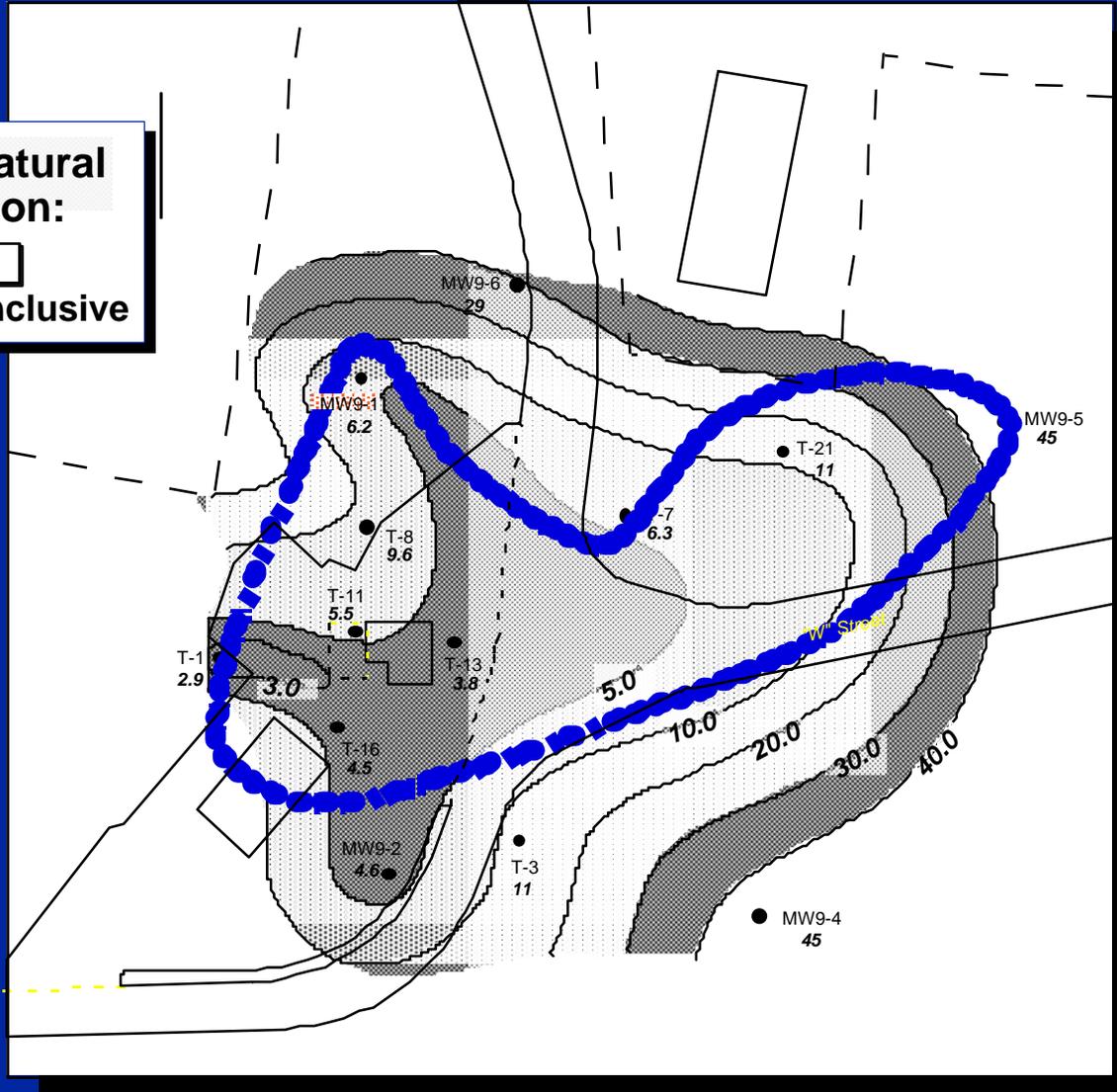


LOW ----- HIGH

# Sulfate in Groundwater (mg/L)

**Supports Natural Attenuation:**

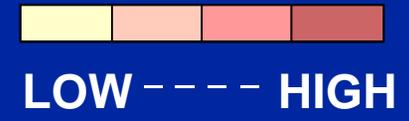
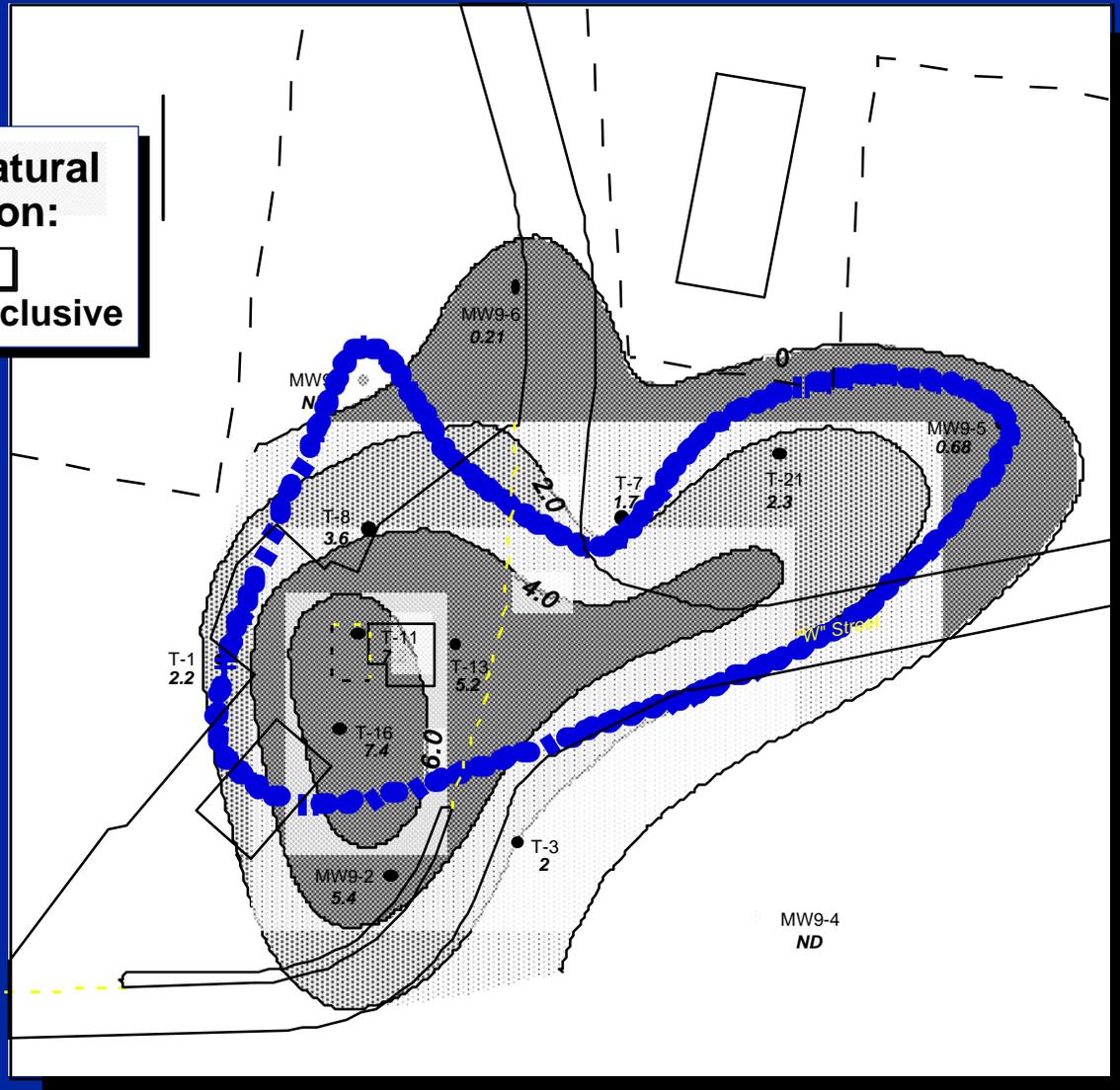
Yes No Inconclusive



# Methane in Groundwater (mg/L)

**Supports Natural Attenuation:**

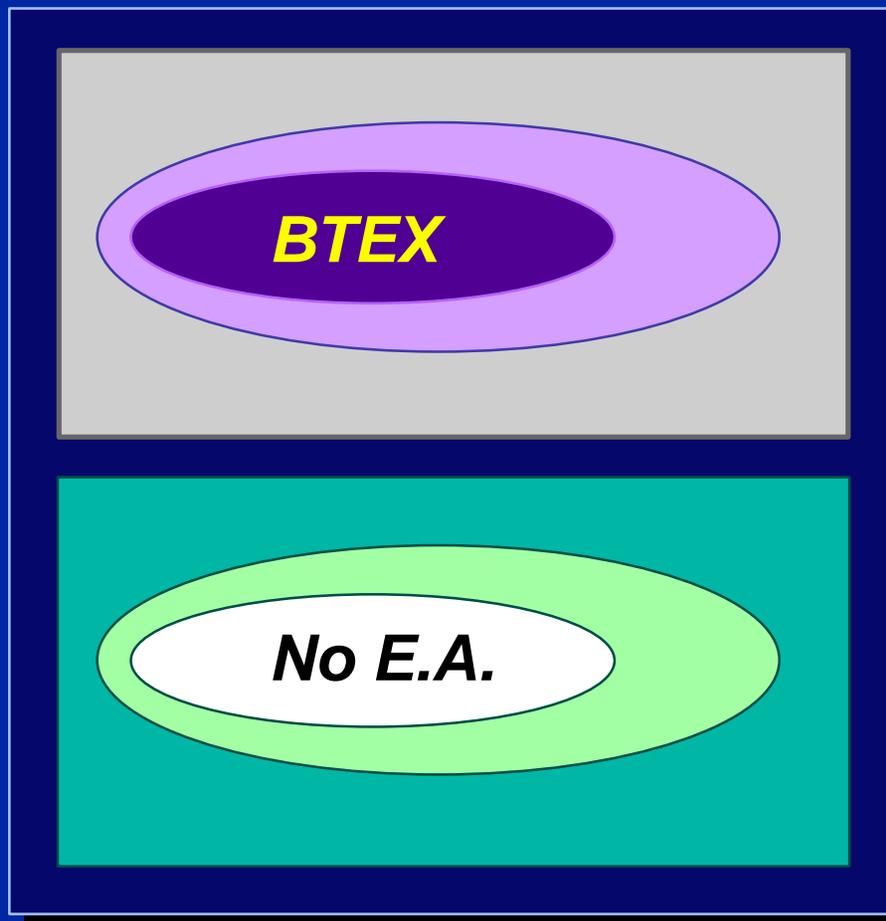
Yes    No    Inconclusive



Electron Acceptor	Type of Reaction	Metabolic By-Product	Redox Potential (pH =7 in volts)	Reaction Preference
■ Oxygen	Aerobic	CO <sub>2</sub>	+ 820	Most Preferred
■ Nitrate	Anaerobic	N <sub>2</sub> , CO <sub>2</sub>	+ 740	↓
■ Ferric Iron (solid)	Anaerobic	Ferrous Iron (dissolved)	- 50	↓
■ Sulfate	Anaerobic	H <sub>2</sub> S	- 220	↓
■ Carbon Dioxide	Anaerobic	Methane	- 240	Least Preferred

# Instantaneous Reaction Model

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Hydrocarbon  
+ Electron Acceptor =

*Electron Acceptor Only, or  
Hydrocarbon Only*

# Instantaneous or Electron-Acceptor-Limited Reaction

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*The microbial reaction is assumed to occur much faster than the time required to replenish the electron acceptor by groundwater flow.*

*Only holds for **Fuel Sites (BTEX plumes)**!*

<b><u>Electron Acceptor or By-Product</u></b>	<b><u>Utilization Factor *</u></b> ( Mass E. Acceptor / By-Prod. Consumed per Mass Dissolved Hydrocarbon Degraded )
Oxygen	3.14 gm/gm
Nitrate	4.9 gm/gm
Ferrous Iron	21.8 gm/gm
Sulfate	4.6 gm/gm
Methane	0.78 gm/gm

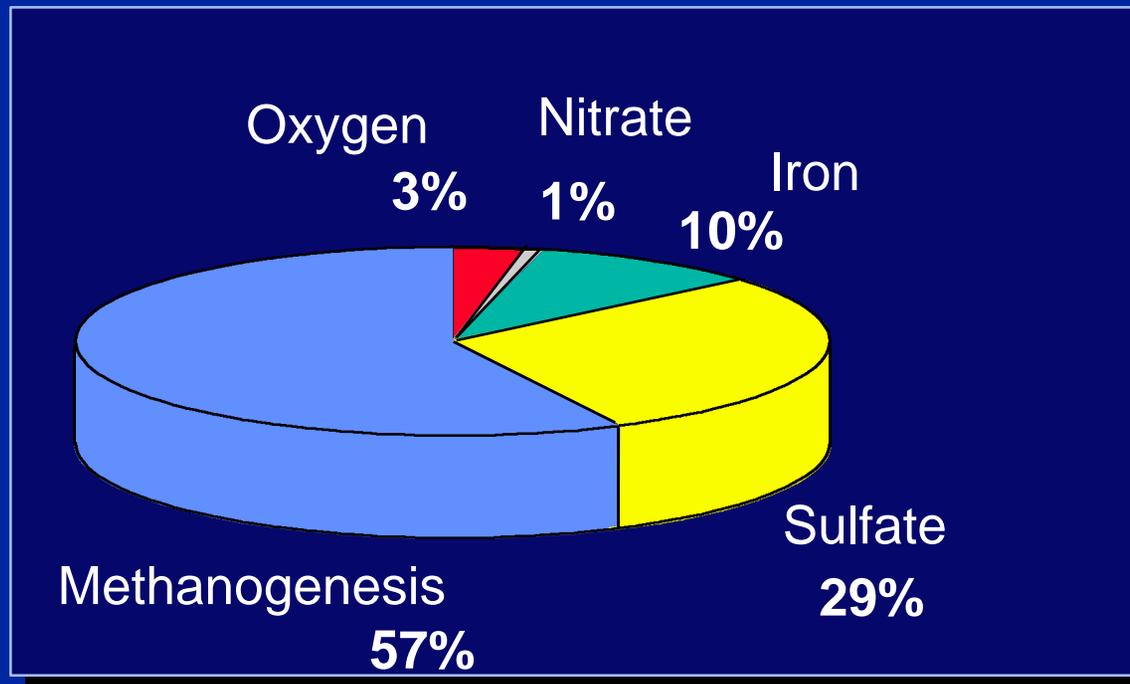
\* Based on BTEX

# Biodegradation Capacity: 16.7 mg/L

CONCENTRATIONS (mg/L)	D.O.	NO <sub>3</sub>	Iron	SO <sub>4</sub>	CH <sub>4</sub>
■ Background	2	0.7	0.5	26.2	0
■ Source	0.4	0	36.6	3.8	7.4
■ Utilization Factor	3.14	4.9	21.8	4.6	0.78
<b>BIODEG. CAPAC.</b>	<b>0.5</b>	<b>0.1</b>	<b>1.7</b>	<b>4.9</b>	<b>9.5</b>

# Contribution to Biodegradation Capacity

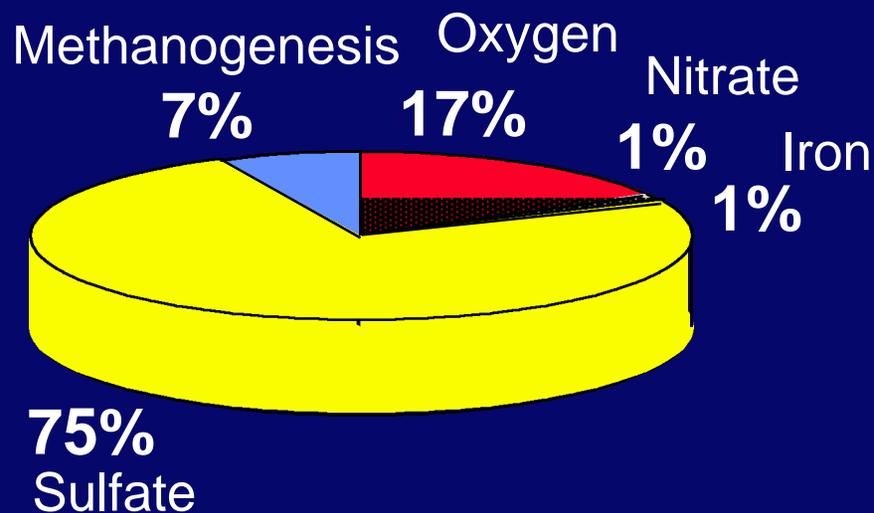
## SWMU 66 KEESLER AFB, MISSISSIPPI



TOTAL BC: 16.7 mg/L

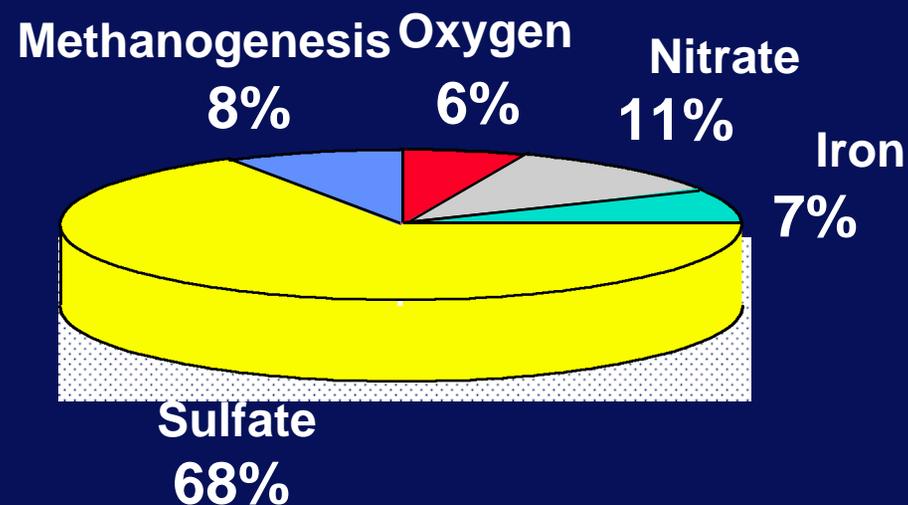
# Contribution to Biodegradation Capacity

**Bldg. 735,  
GRISSOM AFB, INDIANA**



**TOTAL BC: 17.4 mg/L**

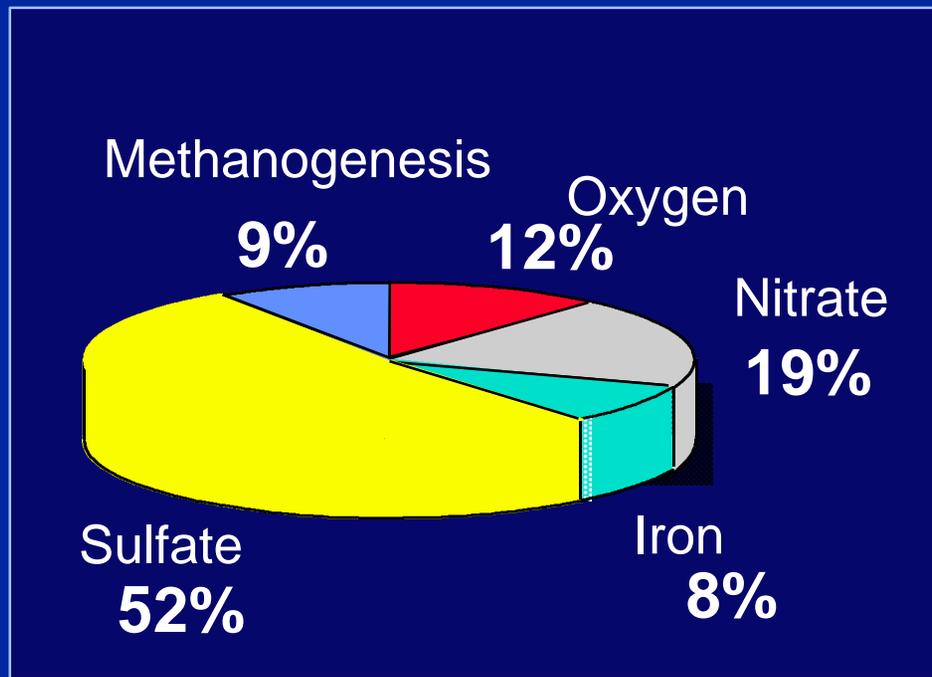
**POL Site,  
HILL AFB, UTAH**



**TOTAL BC: 31.6 mg/L**

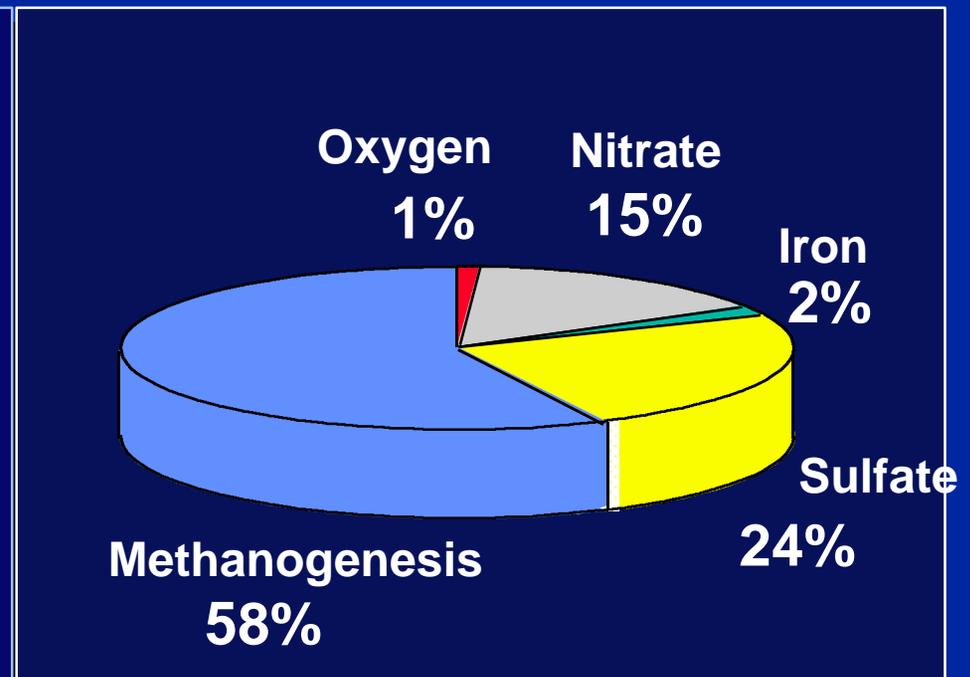
# Contribution to Biodegradation Capacity

## Site ST-41, ELMENDORF AFB, ALASKA



**TOTAL BC: 23.3 mg/L**

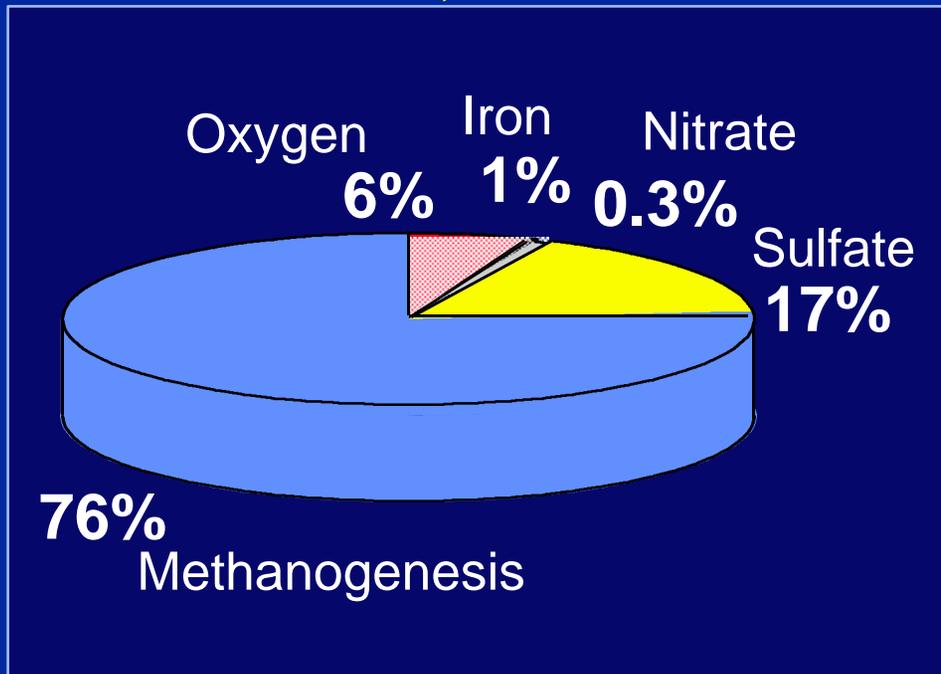
## Hangar 10 Site, ELMENDORF AFB, ALASKA



**TOTAL BC: 20.6 mg/L**

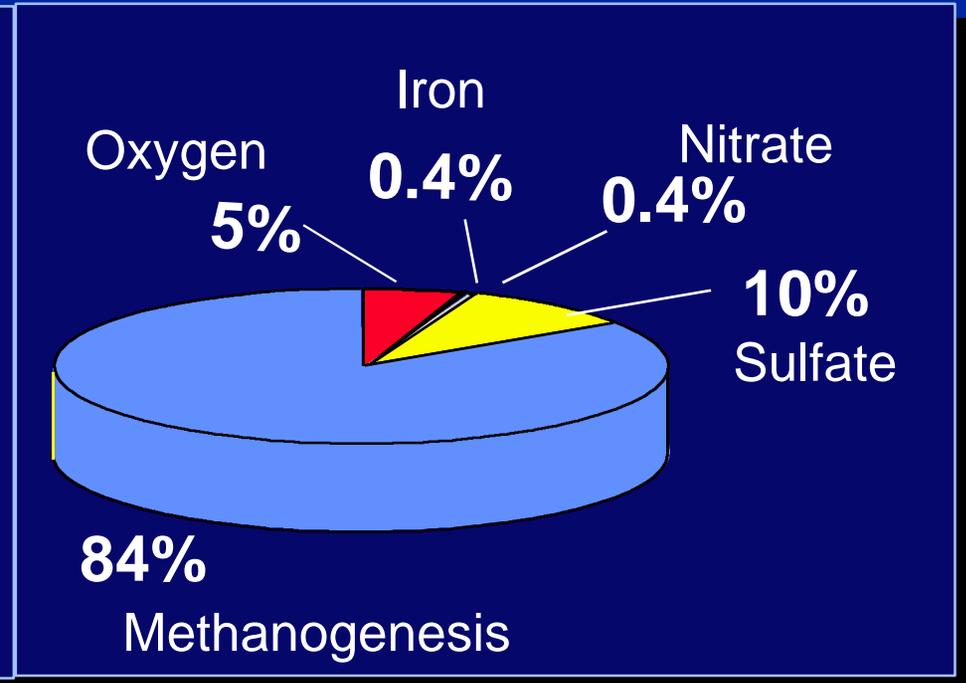
# Contribution to Biodegradation Capacity

## POL B, TYNDALL AFB, FLORIDA



**TOTAL BC: 7.7 mg/L**

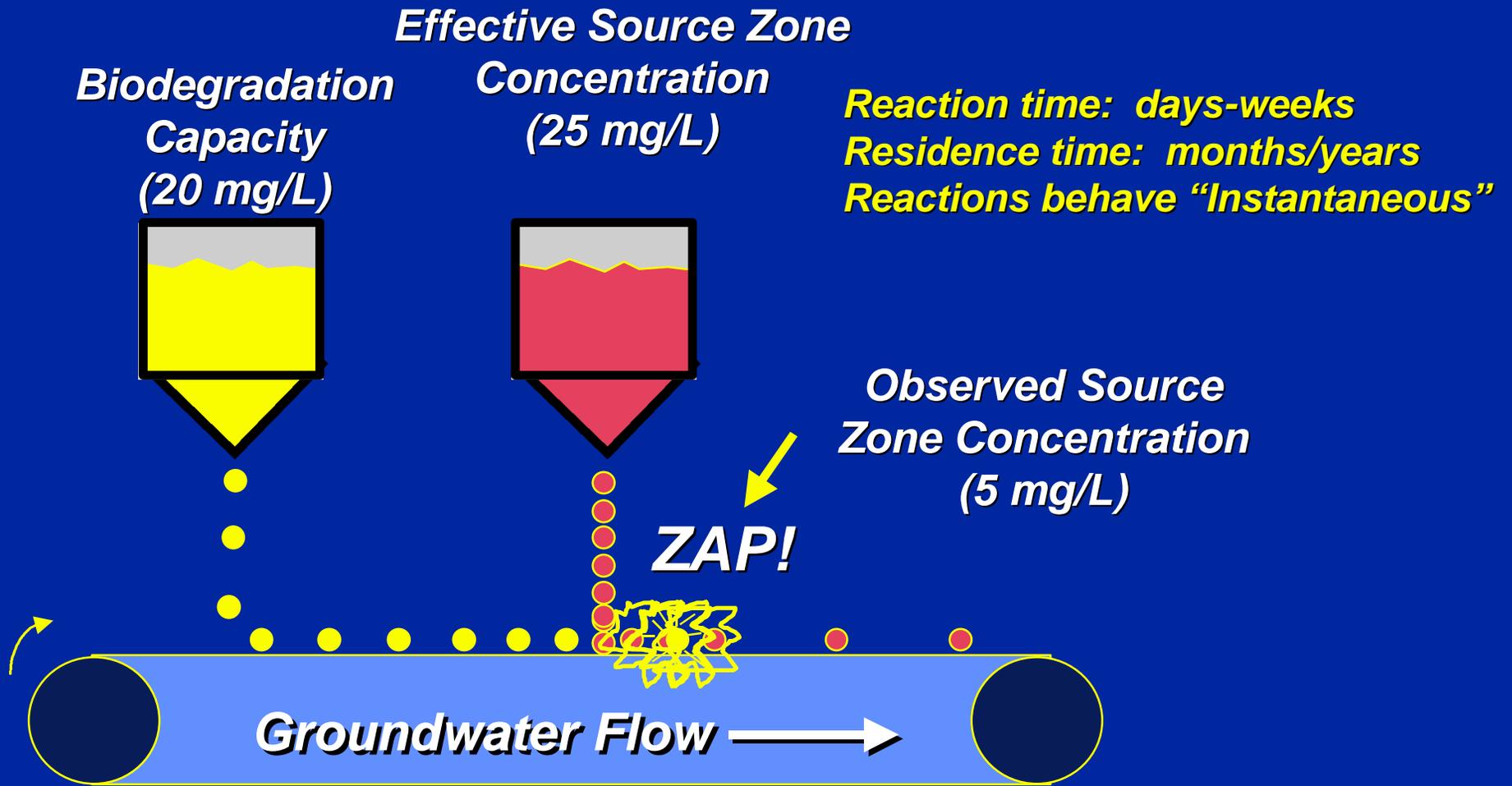
## Site ST-29, PATRICK AFB, FLORIDA



**TOTAL BC: 23.1 mg/L**

# Electron-Acceptor-Limited Biodegradation

## Conceptual Model



# Biodegradation Capacity

## *Options:*

1. Measure in Field
2. Use Typical Values from BIOSCREEN Manual or Literature

Range of Biodegradation Capacity:

**26 Air Force Sites:** 7 to 70 mg/L

**Median 26 Sites = 28.5 mg/L**

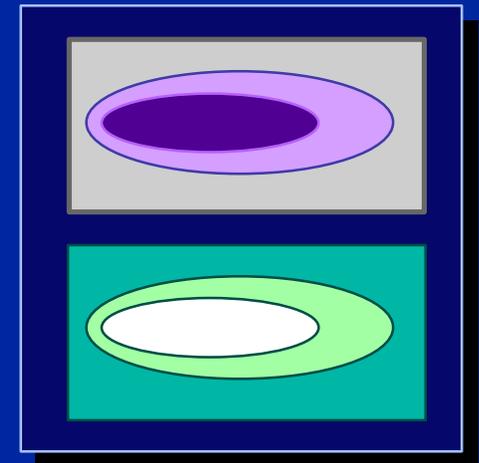
**Median 6 sites Florida = 16.6 mg/L**



# Instantaneous Reaction Model: *Summary*

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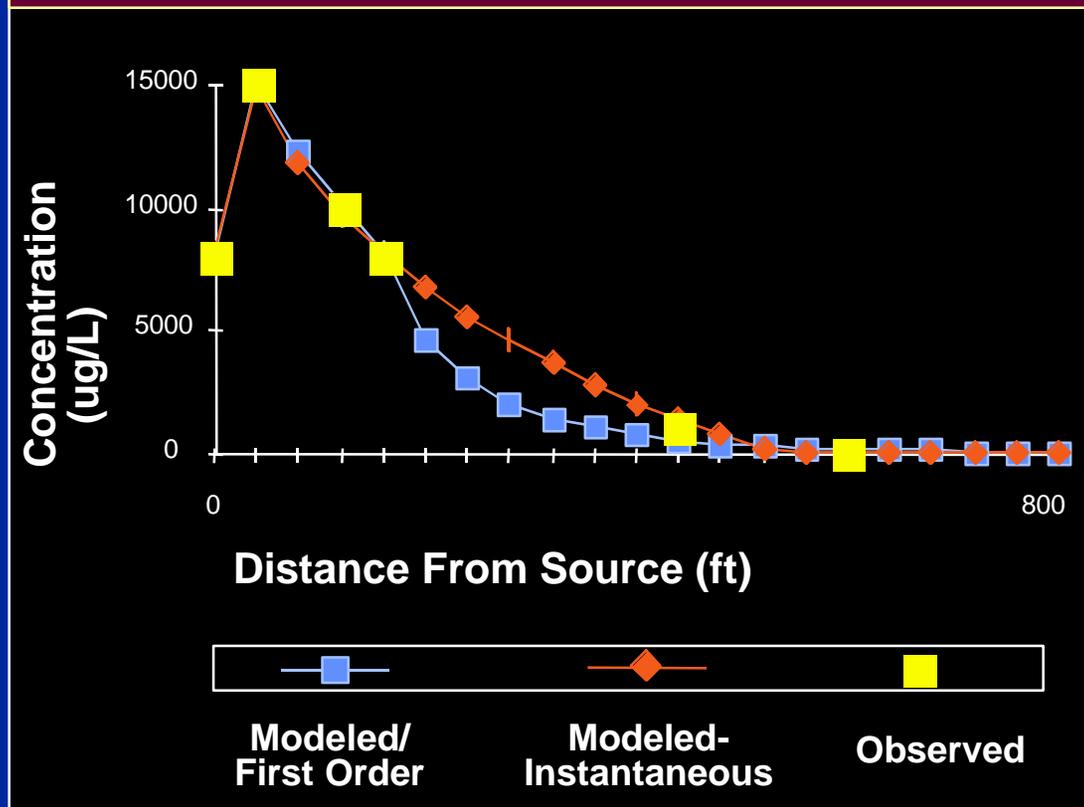
- Assumes microbial kinetics relatively fast
- “Fast” related to residence time in plume
- Transport limited by availability of electron acceptors
- Accounts for electron acceptor reactions in source zone



# BIOSCREEN Modeling Results

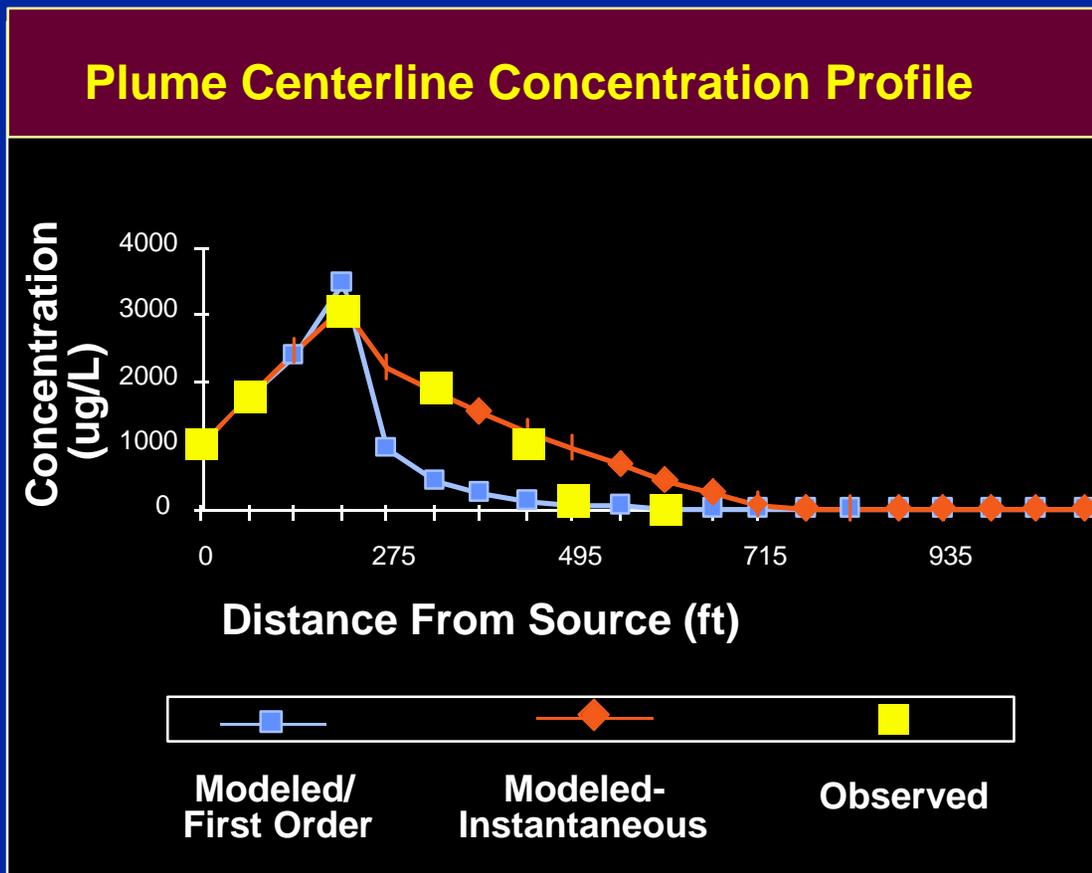
## POL Site / Hill AFB

### Plume Centerline Concentration Profile



# BIOSCREEN Modeling Results

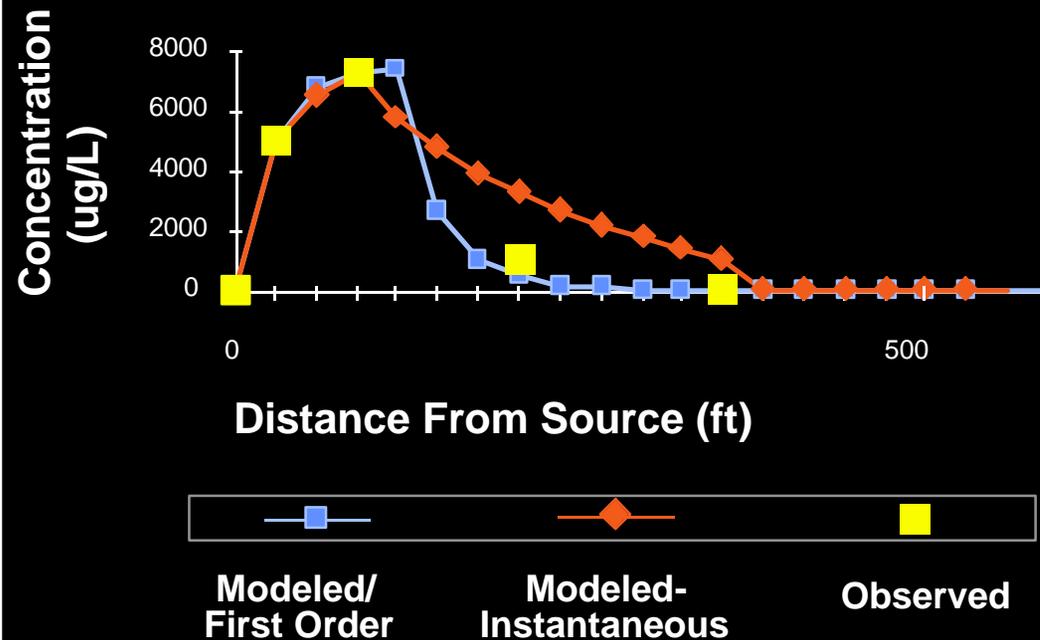
## ST-41 Site / Elmendorf AFB



# BIOSCREEN Modeling Results

## ST-29 Site / Patrick AFB

### Plume Centerline Concentration Profile

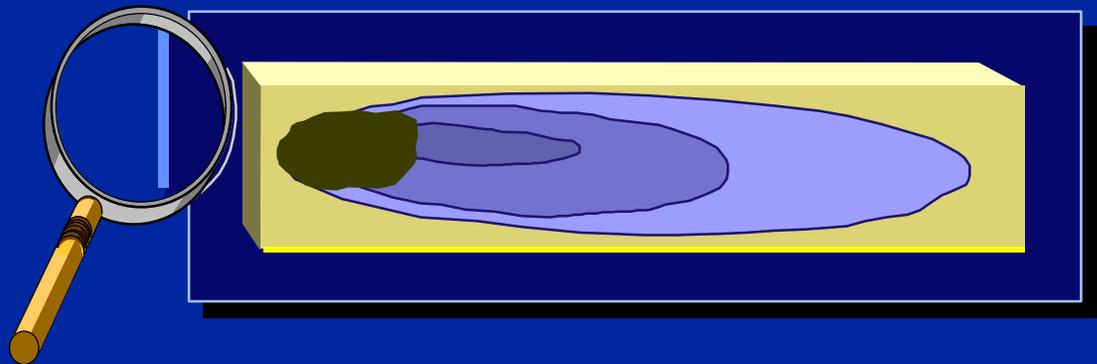


# *Modeling Natural Attenuation with*

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# **BIOSCREEN**

*GROUNDWATER  
SERVICES, INC.*

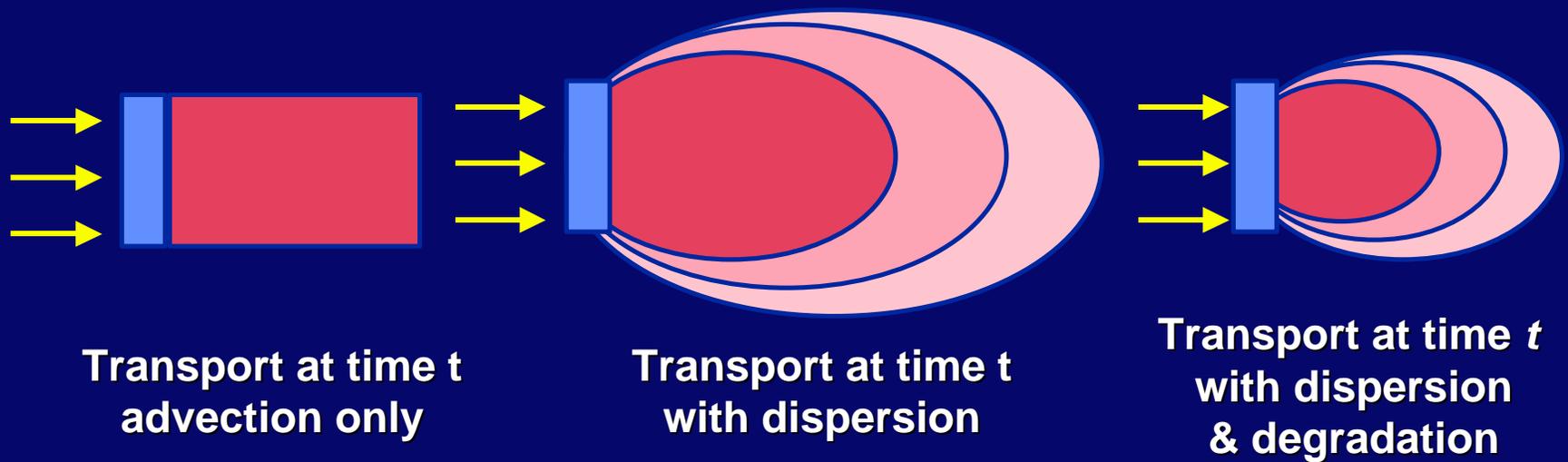


# Groundwater Transport Processes

## Groundwater Transport Modeling

All groundwater transport models are based on the advective-dispersive-reactive equations.

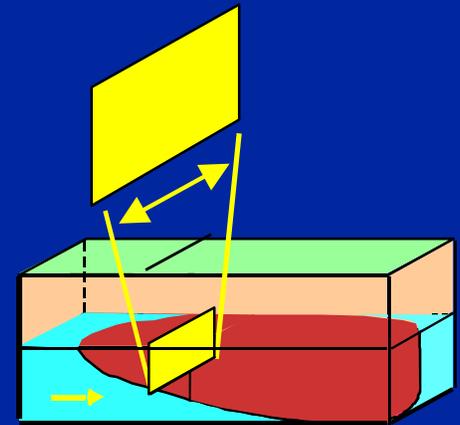
$$\left\{ \begin{array}{l} \text{rate of} \\ \text{change in} \\ \text{HC conc. at} \\ \text{any point} \end{array} \right\} = \left\{ \begin{array}{l} \text{net rate of} \\ \text{advective} \\ \text{transport to} \\ \text{that point} \end{array} \right\} + \left\{ \begin{array}{l} \text{net rate of} \\ \text{dispersive} \\ \text{transport to} \\ \text{that point} \end{array} \right\} - \left\{ \begin{array}{l} \text{net rate of} \\ \text{degradation} \\ \text{at that point} \end{array} \right\}$$



# Types of Fate and Transport Models

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- 1-D vs. 2-D vs. 3-D Advection
- 1-D vs. 2-D vs. 3-D Dispersion
- Deterministic vs. Statistical
- Numerical vs. Analytical
- Transient vs. Steady State
- Constant Source vs. Changing Source



(BIOSCREEN Features)

# Transport: Groundwater in Source Zone → Groundwater at Receptor

Concentration at Downgradient  
Distance  $x$  Away from Source

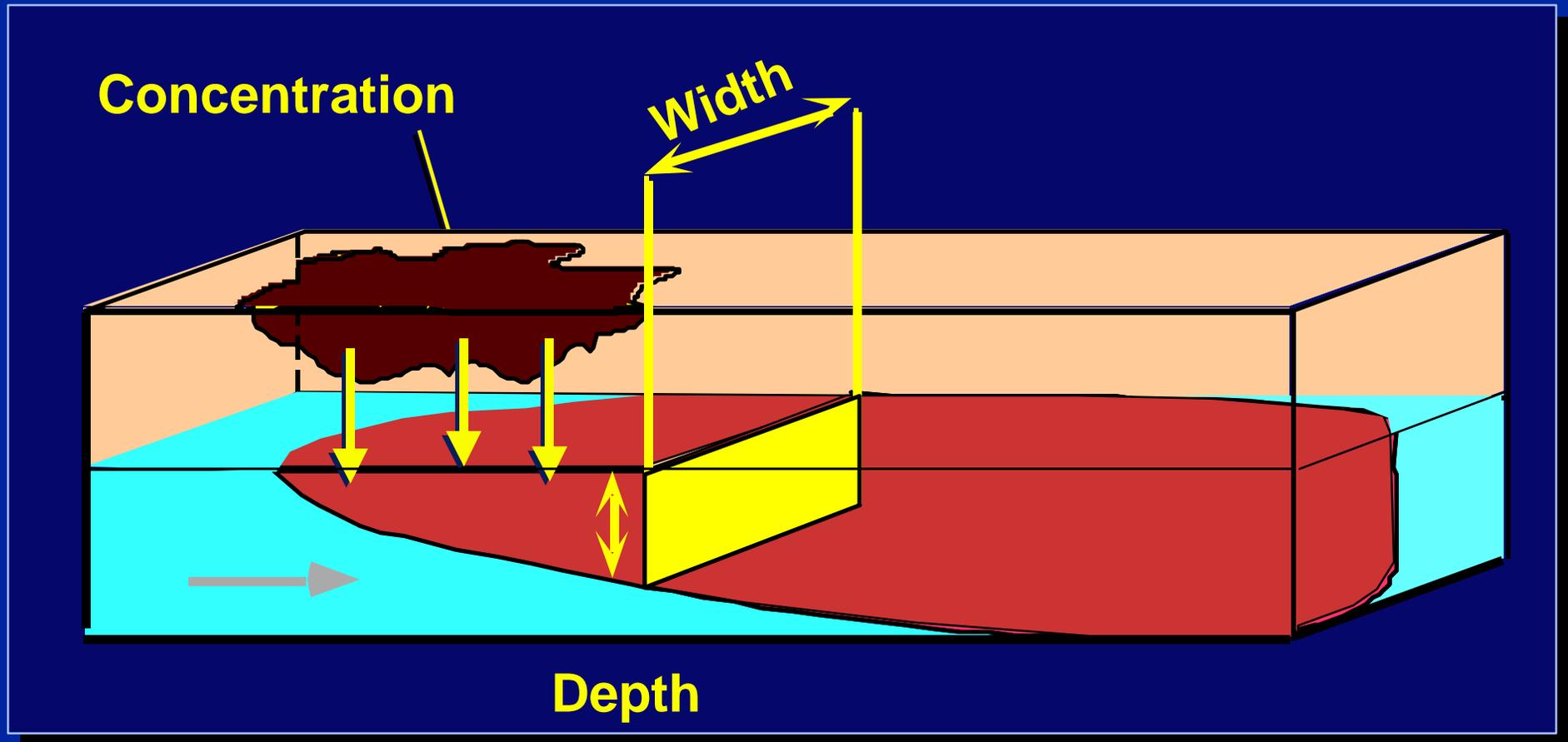
Conc ( $x$ ) =

$$\exp \left\{ \frac{x}{2 a_x} \left[ 1 - \left( 1 + \frac{4 l a_x}{V_s R} \right)^{1/2} \right] \right\} \operatorname{erf} \left[ \frac{S_w}{4 \sqrt{a_y x}} \right] \operatorname{erf} \left[ \frac{S_d}{4 \sqrt{a_z x}} \right]$$

Longitudinal Dispersivity  $a_x$   
 Groundwater Seepage Velocity  $V_s = \frac{K i}{n}$   
 Hydraulic Conductivity  $K$   
 Hydraulic Gradient  $i$   
 Effective Porosity  $n$   
 First-Order Decay Constant  $R$   
 Retardation Factor  $l$   
 Error Function  $\operatorname{erf}$   
 Groundwater Source Width and Depth  $S_w$   
 Transverse Dispersivity  $a_y$   
 Vertical Dispersivity  $a_z$

# Source Term Configuration

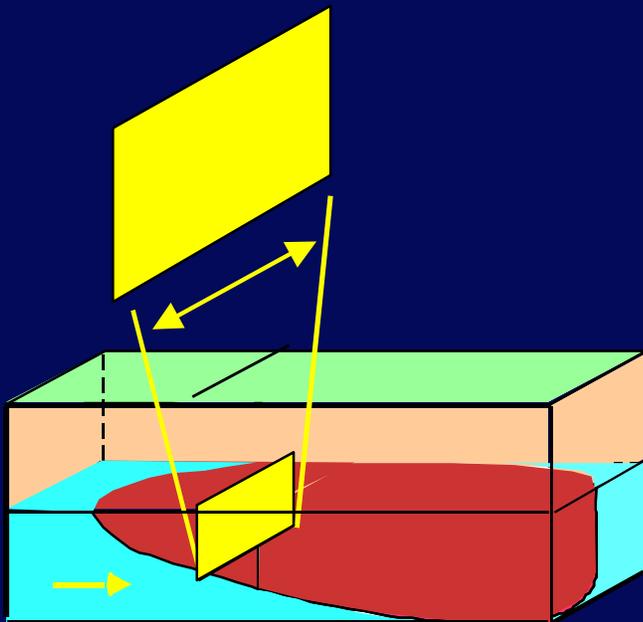
*Location: Downstream of Affected Soil Zone*



# BIOSCREEN Model: *Other Features*

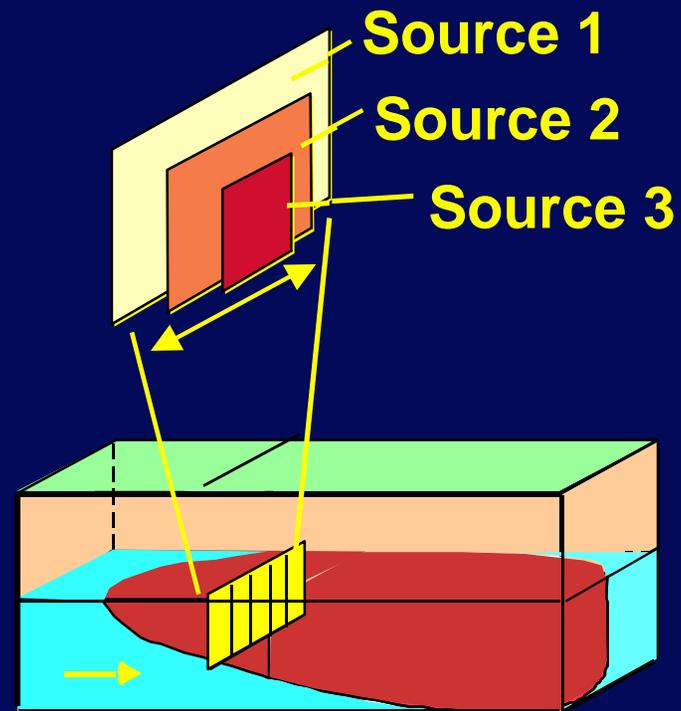
## ■ Single Vertical Plane Source

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## ■ Superimposed Sources (Connor et al., 1995)

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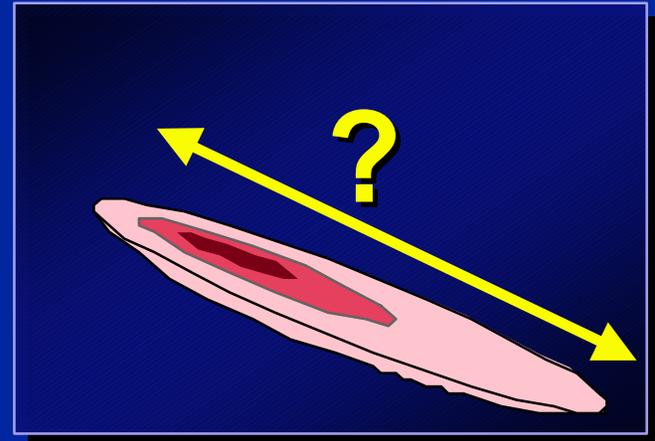


# *How Are Models Used Demonstrate Natural Attenuation?*

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## *Three Viewpoints:*

- **ASTM RNA Standard**
- **EPA Directive**
- **NRC Report**



# ASTM Lines of Evidence for RNA

<b>NRC Data Type</b>	<b>ASTM LINES OF EVIDENCE</b>		<b>Notes</b>
<b>1</b> <i>Measured Loss</i>	<b>Primary</b>	<ul style="list-style-type: none"> <li>■ <i>COC data to define plume as shrinking, stable, or expanding.</i></li> </ul>	<ul style="list-style-type: none"> <li>■ <i>Key evidence for NA</i></li> <li>■ <i>Need historical data</i></li> </ul>
<b>2</b> <i>Evidence of Bio Processes</i>	<b>Secondary</b>	<ul style="list-style-type: none"> <li>■ <i>Geochemical indicators of naturally-occurring biodegradation.</i></li> <li>■ <i>Estimates of attenuation rates.</i></li> </ul>	<ul style="list-style-type: none"> <li>■ <i>ASTM says not needed most UST retail releases</i></li> <li>■ <i>Different rates can be confusing</i></li> </ul>
<b>3</b> <i>Modeling, lab studies, other calcs</i>	<b>Optional (for fuel sites)</b>	<ul style="list-style-type: none"> <li>■ <i>Microbiological studies.</i></li> <li>■ <i>GW solute transport modeling.</i></li> <li>■ <i>Estimates of assimilative capacity.</i></li> </ul>	<ul style="list-style-type: none"> <li>■ <i>May not be optional for non-UST retail sites (EPA quote)</i></li> <li>■ <i>Lab studies done very infrequently</i></li> </ul>

**KEY POINT:** Follow a weight of evidence approach, applying secondary and optional lines of evidence as appropriate.

# EPA MNA Directive: Lines of Evidence

<i>Line of Evidence</i>	<i>Approach</i>
<b>1</b> <i>Historical Trends</i>	<ul style="list-style-type: none"><li>■ <i>Show “clear and meaningful” trend of decreasing contaminant mass and/or concentration vs. time</i></li></ul>
<b>2</b> <i>Indirect Hydrogeologic/Geochemical Data</i>	<ul style="list-style-type: none"><li>■ <i>Shows the type of natural attenuation processes active at a site, and the rate which such processes will reduce contaminant concentrations to required levels.</i></li></ul>
<b>3</b> <i>Direct Microbial Evidence</i>	<ul style="list-style-type: none"><li>■ <i>Directly demonstrates occurrence of a particular attenuation process</i></li></ul>

**KEY POINT:** Probably need both #1 and #2 lines of evidence.

# Computer Models In EPA MNA Directive

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.....a computer model may be helpful for understanding and visualizing current site conditions or for predictive simulations of potential future conditions. Computer models, which simulate site processes mathematically, should in turn be based upon sound conceptual site models to provide meaningful information. Computer models typically require a lot of data, and the quality of the output from computer models is directly related to the quality of the input data. Because of the complexity of natural systems, models necessarily rely on simplifying assumptions that may or may not accurately represent the dynamics of the natural system. Calibration and sensitivity analyses are important steps in appropriate use of models. Even so, the results of computer models should be carefully interpreted and continuously verified with adequate field data.

# National Research Council MNA Report

<b>Requirements</b>	<b>Approach</b>			
<b>1</b> <b>Evaluate “Footprints” of NA Processes</b>	<ul style="list-style-type: none"> <li>■ <i>Identify trends in footprint concentrations</i></li> <li>■ <i>Possibly do mass balances of footprints</i></li> </ul>			
<b>2</b> <b>Analyze Site Data</b>	<b>Recommended level of analysis:</b>	Biodegrades Under Most Conditions (e.g., BTEX)	Biodegrades Under Limited Conditions (e.g., solvents)	Mobile and Degrades Slowly (e.g., MTBE)
	Simple flow, uniform geochemistry, AND low concs	<b>GS</b>	<b>MB</b>	<b>MB + SM</b>
	Simple flow, small-scale physical or chemical heterog., AND med. To high concs.	<b>MB</b>	<b>MB + SM</b>	<b>CM</b>
	Strongly transient flow, large- scale physical or chemical heterog., OR high concs.	<b>MB or SM</b>	<b>CM</b>	<b>CM</b>

- *Graphical and statistical analysis= **GS***
- *Simple Modeling= **SM***
- *Mass budgeting to track fate of  
contaminants = **MB***
- *Compreh. Modeling= **CM***

# Computer Models In NRC Report

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**Models are the “...highest level of analysis for natural attenuation site data...”**

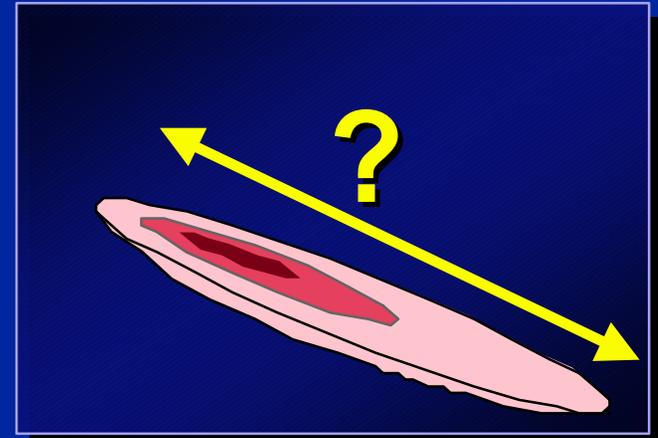
**“For sites at which degradation products are straightforward and hydrogeology is relatively simple a budget analysis combined with simple solute transport modeling often is adequate. On the other hand, as biochemical or hydrogeological characteristics become more complex, analysis of the site requires the rigor of comprehensive models.”**

# What Goes Into an MNA Report?

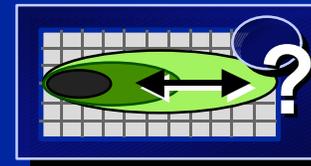
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## *Combined Viewpoint:*

- Concentration vs. Time Data
- “Footprint” Data
- Modeling Results



# Third L.O.E.: How are Models Used to Demonstrate MNA?



## **Method 1.**

**Use model to show plume is shrinking or stable**

### *Step 1*

**Calibrate model to existing monitoring data.**

### *Step 2*

**Increase time to 100 years in the future.**

### *Step 3*

**See if plume gets larger.**

## **Method 2.**

**Use model to link biodegradation to footprints**

### *For BTEX plumes:*

**Model with Electron Acceptor Limited Biodegradation and Fit Model to Site Data**

### *For Chlorinated Solvent plumes:*

**Model with Sequential Reductive Dechlorination to Generate Daughter Product, Match to Site Data**

# Why Use Models?

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◆ Method for Predicting Something Precisely ? **No**

- ➔ ◆ System to Organize Site Data . . . . . **Yes**
- ➔ ◆ Tool to Help Understand Site Processes . **Yes**
- ➔ ◆ Additional Line of Evidence . . . . . **Yes**
- ➔ ◆ Screen for Applicability of MNA . . . . . **Yes**

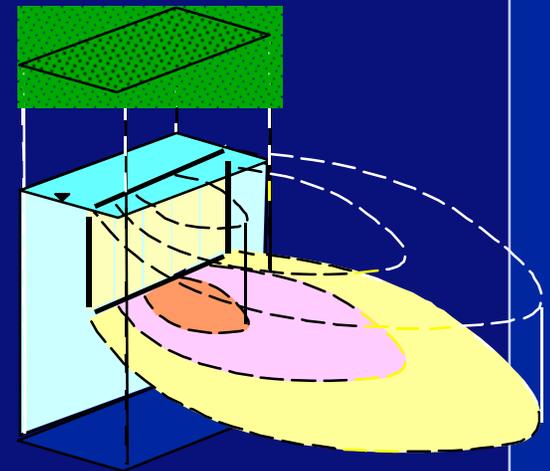
# Model Selection Guidelines

Model Type	Capabilities	Data Needs	Complexity
■ <b>Hand Calcs:</b>	Advection Only	Simple	 <p>"Gilligan"</p>
■ <b>Analytical (BIOSCREEN BIOCHLOR):</b>	Uniform flow Simple source Key NA Processes	Moderate	 <p>"Skipper"</p>
■ <b>Numerical Model (BIOPLUMEIII):</b>	Complex flow Complex sources Pumping	High	 <p>The "Professor"</p>

# Natural Attenuation Models

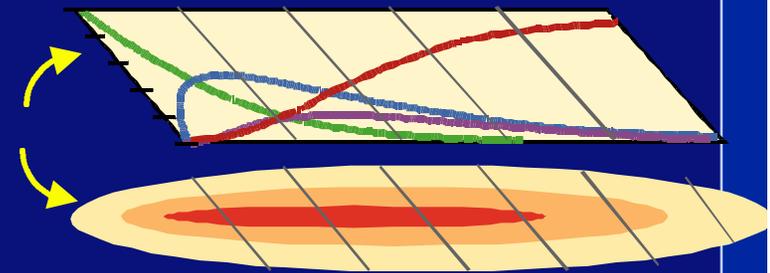
## Fuel Sites

- ➔ BIOSCREEN (*analytical, two decay options, source decay term*)
- BIOPLUME III (*numerical, electron acceptors*)



## Solvent Sites

- ➔ BIOCHLOR (*analytical, sequential reductive dechlorination*)
- RT3D (*complex numerical model*)



# Where to Get **BIOSCREEN**

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## EPA Center for Subsurface Modeling Support (R. S. Kerr Lab)

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- **Web:**  
<http://www.epa.gov/ada/bioscreen.html>
- **Phone**  
(405) 436 8718



# Natural Attenuation Tools

Line of Evidence	Excel	Mapping SW, CAD	MAROS	Fate 5	Seq- uence	BIO- SCREEN	BIO- CHLOR	BIOPLUMEIII RT3D	BIOSOURCE
<b>Primary</b> <ul style="list-style-type: none"> <li>■ Plotting C vs. T</li> <li>■ Mann-Kendall, Mann-Whitney Stats</li> </ul>	3 3*	3 *	3 3						
<b>Secondary</b> <ul style="list-style-type: none"> <li>■ Plotting geochemical indicators</li> <li>■ Estimation of attenuation rates</li> </ul>	3 * 3 *	3 *			3				
<b>Optional</b> <ul style="list-style-type: none"> <li>■ GW solute model</li> <li>■ Soil-to-GW leachate model</li> <li>■ Calculation of Time to Natural Attenuate</li> <li>■ Assimilative capacity calc.</li> </ul>						3 *	3		3
<b>3 * = not built-in</b>									
<b>Cost</b>	\$ 200	varies	Free	\$ 250	\$495	Free	Free	Free	Free

# Where to Get Natural Attenuation Software Tools

- **Primary Line of Evidence**

- MAROS ([www.gsi-net.com](http://www.gsi-net.com))

- **Secondary Line of Evidence**

- SEQUENCE ([www.rovers.com](http://www.rovers.com) - see innovations) (\$495)

- Fate V ([www.gsi-net.com](http://www.gsi-net.com)) (\$295)

- **Models**

- BIOSCREEN ([www.epa.gov/ada/models.html](http://www.epa.gov/ada/models.html)) (free)

- BIOPLUME III ([www.epa.gov/ada/models.html](http://www.epa.gov/ada/models.html)) (free)

- BIOCHLOR ([www.epa.gov/ada/models.html](http://www.epa.gov/ada/models.html)) (free)

- RT3D (<http://terrassa.pnl.gov:2080/bioprocess/rt3d.ht>) (free)